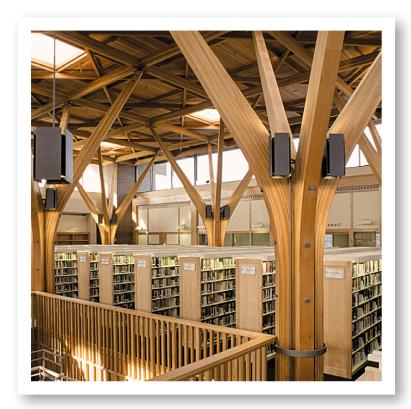
ANSI 117-2015

AMERICAN NATIONAL STANDARD

Standard Specification for Structural Glued Laminated Timber of Softwood Species







AMERICAN NATIONAL STANDARD

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Standard Specification for Structural Glued Laminated Timber of Softwood Species

APA – The Engineered Wood Association

Approved April 17, 2015 American National Standards Institute

FOREWORD (This Foreword is not a part of American National Standard ANSI 117-2015)

This Standard is an American National Standard previously designated as ANSI 117-2010. It contains information for the design of structural glued laminated timber (glulam) members.

Since January 1, 2013, APA – The Engineered Wood Association has assumed the Secretariat responsibilities for this Standard. The maintenance of this Standard follows the Operating Procedures for Development of Consensus Standards of APA – The Engineered Wood Association, approved by ANSI.

Inquiries or suggestions for improvement of this standard are welcome and should be directed to *APA – The Engineered Wood Association* at 7011 South 19th Street, Tacoma, WA 98466, www.apawood.org.

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ANSI 117-2015 STANDARD SPECIFICATION FOR STRUCTURAL GLUED LAMINATED TIMBER OF SOFTWOOD SPECIES

PREFACE

The term *structural glued laminated timber* (glulam) as used herein refers to an engineered, stress-rated product of a timber laminating plant, comprising assemblies of suitably selected and prepared wood laminations bonded together with adhesives. The grain of all laminations is approximately parallel longitudinally. Glulam is permitted to be comprised of pieces end joined to form any length, of pieces placed or bonded edge to edge to make any width, or of pieces bent to curved form during bonding.

This Specification contains values for the design of structural glued laminated timber members. It is, however, intended to be neither a design manual nor an engineering textbook. Structural design of glued laminated timber members and their fastenings shall be in accordance with the National Design Specification® (NDS®) for Wood Construction (15).

Section 1 of this Specification (*Basic Requirements*) identifies characteristics of importance to the use of structural glued laminated timber and provides general information useful to the manufacturer and designer.

Section 2 (*Reference Design Values*) provides and describes reference design values for use in the design of structural glued laminated timber. The reference design values require adjustment by procedures detailed in the NDS.® The design values described herein are for use with the Allowable Stress Design (ASD) methodology. For Load and Resistance Factor Design (LRFD), conversion formulas for design values are provided in the NDS.® The design values of glued laminated timber used in utility structures can be obtained by multiplying the reference design values provided in this Specification by the conversion factors specified in ANSI O5.2 (4).

Specific lay-up requirements are provided in Section 3 of this Specification (*Lay-up Requirements*). The production of structural glued laminated timber under this Specification shall be in accordance with American National Standard ANSI A190.1 *Structural Glued Laminated Timber* (3).

Combinations not listed in this Specification are permitted to be used provided that all other requirements of this Specification are met. Specific requirements for alternate combinations are included in Section 4 of this Specification (*Alternate Combinations*).

1. BASIC REQUIREMENTS

1.1 General

Structural glued laminated timber conforming to this Specification shall be produced in laminating plants audited and licensed by an accredited inspection agency meeting the requirements of ANSI A190.1 (3). Quality assurance for workmanship and materials shall be the responsibility of the manufacturer's quality control operations. The manufacturer's quality control systems shall be subject to periodic auditing by the accredited inspection agency. Timbers conforming to this Specification shall be marked according to ANSI A190.1 (3).

Structural glued laminated timbers are permitted to be made up of a single grade of lumber or multiple grades placed with specific quantities in specific zones within the cross-section. Structural glued laminated timber combinations generally utilize higher grade lumber in the outer zones than in the center of the beam or core. Design values for structural glued laminated timbers are established according to the analysis procedures of ASTM D3737 (9) or through full scale tests in accordance with ASTM D7341 (13) and analysis in accordance with ASTM D2915 (8).

1.2 Species

Structural glued laminated timber can be manufactured from any suitable wood species. Wood species with similar properties are grouped for convenience. Design properties and lay-up information are included in this Specification for structural glued laminated timbers of the following species groups:

Species Group	Symbol	Species that may be included in the group
Alaska Cedar	AC	Alaska Cedar
Douglas-Fir-Larch	DF	Douglas-Fir, Western Larch
Eastern Spruce	ES	Black Spruce, Red Spruce, White Spruce
Hem-Fir	HF	California Red Fir, Grand Fir, Noble Fir, Pacific Silver Fir, Western Hemlock, White Fir
Port Orford Cedar	POC	Port Orford Cedar
Softwood Species	SW	Alpine Fir, Balsam Fir, Black Spruce, Douglas Fir, Douglas Fir South, Engelmann Spruce, Idaho White Pine, Jack Pine, Lodgepole Pine, Mountain Hemlock, Norway (Red) Pine, Ponderosa Pine, Sitka Spruce, Sugar Pine, Red Spruce, Western Larch, Western Red Cedar, White Spruce
Southern Pine	SP	Loblolly Pine, Longleaf Pine, Shortleaf Pine, Slash Pine
Spruce-Pine-Fir ^(a)	SPF	Alpine Fir, Balsam Fir, Black Spruce, Engelmann Spruce, Jack Pine, Lodgepole Pine Norway (Red) Pine, Red Spruce, Sitka Spruce, White Spruce

Other species or species groups are permitted to be used in accordance with ANSI A190.1 (3).

1.3 Combination Symbols

Each structural glued laminated timber lay-up is assigned a combination symbol. The combination symbol is used to identify a combination and to distinguish one combination from another. Each combination is assigned design values based on ASTM D3737 (9) or full scale tests in accordance with ASTM D7341 (13). Design values for combinations are tabulated in *Annex A*. Lay-up requirements for combinations are tabulated in *Annex B*.

The combination symbols in *Table A1-Expanded* indicate the primary design bending stress and the grading system used for the lumber in the outer zones. For example, 24F-V4 indicates that the beam has a primary bending design value of 2400 psi (16.6 MPa) and that the lumber in the outer zones was visually graded. 24F-E13 indicates that the bending design value is 2400 psi (16.6 MPa) and the lumber in the outer zones was

E-rated using a mechanical grading system in addition to visual requirements. The number at the end of the combination symbol (13 in this example) is a number assigned to distinguish between different combinations. The species group(s) used in the beam is also included as part of the combination symbol. The first species group listed corresponds to the laminations in the outer zones of the lay-up, and the subsequent species group is for the laminations used in the interior zones.

The combination symbols for lay-ups in *Table A2* are numbers which have been assigned for specification purposes. Each combination symbol corresponds to a specific grade of lumber used in a uniform grade lay-up.

1.4 Stress Classes

To simplify specification, combinations from *Table A1-Expanded* with similar design stresses have been grouped into stress classes. These stress classes are recommended for specification purposes rather than specifying by combination symbol. Use of the stress class system allows manufacturers flexibility in choosing combinations that make efficient use of their available resources and simplifies the design process. These stress classes are shown in *Table A1*.

Stress classes are designated by primary bending stress and modulus of elasticity. To qualify for a stress class, combinations are required to have design values that meet or exceed all values listed for the stress class. Each combination qualifying for a stress class also qualifies for all lower stress classes.

Because the stress classes are not species-group-specific, it is critical that the designer specify when a particular species is required for appearance reasons or other considerations. Some stress classes are not available in all species. *Table A1-Expanded* lists combinations included in each stress class.

1.5 Balanced or Unbalanced Lay-ups

Structural glued laminated timbers are permitted to be manufactured with lumber grades placed symmetrically or asymmetrically about the neutral axis of the member. Timbers with symmetric lay-ups are referred to as "balanced" and have the same design values for positive and negative bending. Timbers with asymmetric lay-ups are referred to as "unbalanced" and have higher design stresses for positive bending than for negative bending. Unbalanced lay-ups are generally used for simple, single-span beams, while balanced lay-ups are used for continuous or cantilevered beams. Unbalanced combinations are permitted to be used as continuous or cantilevered beams, provided that the stresses due to negative moment do not exceed the tabulated bending design value modified by applicable adjustment factors. The top side of straight or cambered beams is required to be marked "TOP" by the manufacturer to facilitate proper installation.

1.6 Adjusted Design Stresses

Reference design stresses for structural glued laminated timber are based on standard conditions and must be modified for expected end-use conditions by applying adjustment factors from the NDS® (15). The reference design stress multiplied by all applicable adjustment factors is referred to as the "adjusted design stress." The reference design values are discussed in Section 2.

1.7 Standard Sizes

ANSI A190.1 (3) permits the use of any width or depth of structural glued laminated timber. The use of standard finished sizes constitutes recommended practice to the extent that other considerations will permit. The depth and width of the timber shall be as agreed upon by the buyer and seller. All members shall be sized in accordance with the width, depth, and length requirements of the structural design. Dimensional tolerances shall be in accordance with ANSI A190.1 (3).

Standard net finished widths for structural glued laminated timbers are as shown in Table 1.7.

STANDARD NET FINISH	HED WIDTHS FOR STRUCTURAL GLUED LAMI	NATED TIMBER
Nominal Width of Laminations	Softwoods Other Than Southern Pine Net Width (in.)	Southern Pine Net Width (in.)
3	2-1/8 (55 mm) or 2-1/2 (65 mm)	2-1/8 (55 mm) or 2-1/2 (65 mm)
4 (a)	3-1/8 (80 mm)	3 (75 mm) or 3-1/8 (80 mm)
6(a)	5-1/8 (130 mm)	5 (125 mm) or 5-1/8 (130 mm)
8	6-3/4 (170 mm)	6-3/4 (170 mm)
10	8-3/4 (220 mm)	8-1/2 (215 mm)
12	10-3/4 (275 mm)	10-1/2 (265 mm)
14	12-1/4 (310 mm)	12 (305 mm)
16	14-1/4 (360 mm)	14 (355 mm)

Standard depths are in multiples of the standard lamination thickness. Southern pine laminations are typically surfaced to 1-3/8 inches (35 mm) thick, and laminations of other softwood species are typically surfaced to 1-1/2 inches (38 mm) thick. Laminations 3/4 inch (19 mm) thick are often used for curved members of both southern pine and western species. Depths matching standard I-joist depths are also available from many

1.8 Shapes

manufacturers.

Structural glued laminated timbers can be manufactured in a variety of shapes from straight beams to curved arches. Members can also be manufactured with tapered or constant cross section.

- **1.8.1** For curved members manufactured with nominal 2-inch thickness laminations, the minimum radius of curvature (at the inside face) is 18 feet for southern pine and 27 feet 6 inches for other softwood species.
- **1.8.2** For tudor arches and other tightly curved members manufactured with nominal 1 inch thickness laminations, minimum radii of curvature (at the inside face) are:

7 feet 0 inch* for southern pine

9 feet 4 inches* for all other softwood species

1.9 Appearance Grades

Appearance grades shall be specified in accordance with ANSI A190.1 (3) or as agreed upon between buyer and seller. The reference design values are independent of the appearance grades.

Special surfacing, such as rough saw texturing, may reduce the cross section and may affect the member capacity based on the reduced section properties. The reduced cross section (if applicable) shall be considered in design.

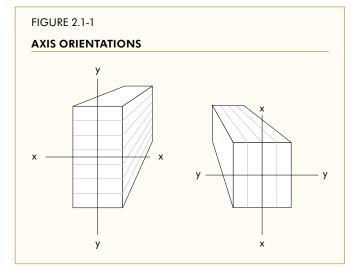
^{*}The manufacture of curved members with radii shorter than these requires standard thickness laminations to be planed to a thinner dimension resulting in more waste and less efficient use of materials. It is recommended that the designer contact the laminator prior to specifying radii shorter than those listed above. For thin laminations, the radius shall not be less than 100 times the lamination thickness for southern pine or 125 times the lamination thickness for other softwoods.

2. REFERENCE DESIGN VALUES

2.1 General

Design values for structural glued laminated timber are dependent on the orientation of the member relative to the applied loads. Values designated with a subscript "x" are based on transverse loads applied perpendicular to the wide faces of the laminations, causing bending about the x-x axis (Figure 2.1-1). Values designated with a subscript "y" are based on transverse loads applied parallel to the wide faces of the laminations, causing bending about the y-y axis (Figure 2.1-1).

Design values are tabulated for bending $(F_{bx}^+, F_{bx}^-, F_{by})$, compression perpendicular to grain $(F_{c\perp x}, F_{c\perp y})$, shear (F_{vx}, F_{vy}) , modu-



lus of elasticity (E_x, E_y) , tension parallel to grain (F_t) , and compression parallel to grain (F_c) . Also tabulated are specific gravity values and species groups for use in connection design. Values are not tabulated for torsion, for modulus of rigidity, or for radial stresses in curved bending members, because these values can be determined from other tabulated design values.

2.2 Bending Design Values, F_{bx}+, F_{bx}-, F_{by}

Tabulated design values are provided for positive bending of horizontally laminated timbers (F_{bx}^+), negative bending of horizontally laminated timbers (F_{bx}^-), and bending of vertically laminated members (F_{by}). Horizontally laminated members have bending loads applied perpendicular to the wide faces of the laminations. Vertically laminated members have bending loads applied parallel to the wide faces of the laminations. Positive bending causes tensile stresses at the bottom of a beam. Negative bending causes compressive stresses at the bottom of a beam.

2.3 Compression Perpendicular to Grain Design Values, $F_{c\perp x}$, $F_{c\perp y}$

The use of multiple laminating grades results in different design values in compression perpendicular to grain for the top and bottom and for the side faces of a beam. One value is tabulated for use in bearing on the top or bottom of the beam and one value is tabulated for side bearing to simplify design.

The tabulated compression perpendicular to grain design values are based on a deformation limit of 0.04 inch (1 mm) obtained when tested in accordance with ASTM D143 (6). A compression perpendicular to grain design value based on a 0.02 inch (0.5 mm) deformation limit can be estimated as 73% of the tabulated value.

2.4 Shear Design Values, F_{vx}, F_{vv}

The tabulated shear design values, F_{vx} and F_{vy} , are permitted to be used for prismatic members subjected to most load conditions. For non-prismatic members and for all members subject to impact or cyclic loads, the reference shear values shall be 72% of the tabulated values. The reduced value shall also apply to the design of members to resist shear from mechanical fasteners.

Prismatic members shall be defined as straight (or cambered) members with constant cross section. Non-prismatic members include, but are not limited to: arches, tapered beams, curved beams, and notched members.

The tabulated shear design values, F_{vy} , are applicable to members with four or more laminations. For members with three laminations, the reference design value shall be 95% of the tabulated value. For members with two laminations, the reference design value shall be 84% of the tabulated value.

The tabulated shear design values permit minor amounts of checking (\leq 15% of beam width) without explicit consideration by the designer. An accredited inspection agency will typically provide guidelines for the analysis of severely checked beams.

Modulus of Elasticity Design Values, $E_{x \text{ true}}$, $E_{x \text{ app}}$, $E_{x \text{ min}}$, $E_{y \text{ true}}$, $E_{y \text{ app}}$, $E_{y \text{ min}}$, E_{axial} , and $E_{axial \text{ min}}$ Design values for modulus of elasticity (E) are tabulated for bending about either axis (x-x or y-y, as shown in Figure 2.1-1). In general, the apparent moduli of elasticity, $E_{x \text{ app}}$ and $E_{y \text{ app}}$, are used for calculation of deflection of bending members, and $E_{x \text{ min}}$ and $E_{y \text{ min}}$ are used for stability calculations for columns and beams.

 $E_{x \, app}$ and $E_{y \, app}$ are based on a span to depth ratio of 21, including an adjustment for shear deflection. These values can be used for most designs without considering shear deflections explicitly. For span-to-depth ratios of less than 14, deflections due to shear stresses should be considered. ASTM D2915 (8) presents one method of accounting for shear deflections.

 $E_{x\,true}$ and $E_{y\,true}$ are shear-free moduli of elasticity and generally estimated as 1.05 $E_{x\,app}$ and 1.05 $E_{y\,app}$, respectively. When $E_{x\,true}$ and $E_{y\,true}$ are used, the calculated deflection of members accounts for the deflection due to bending only and therefore, the deflection due to shear must be calculated separately and then added to the bending deflection to account for the total deflection of the members.

For the calculation of extensional deformations, the axial modulus of elasticity for mixed grade lay-up combinations provided in *Tables A1* and *A1-Expanded* can be estimated as $E_{axial} = 1.05 E_{y\,app} = E_{y\,true}$, such as for use in calculating deflection of trusses. The bending modulus of elasticity for uniform grade lay-up combinations provided in *Table A2* can be estimated as $E_{x\,true} = E_{y\,true} = E_{axial}$, and $E_{x\,app} = E_{y\,app} = 0.95 E_{axial}$.

 $E_{x\,min},\,E_{y\,min},$ and $E_{axial\,min}$ are calculated using the following formula:

$$E_{\min} = \frac{E_{app} \left[1 - 1.645 (CoV_E)\right] [1.05]}{1.66} = \frac{E_{app} \left[1 - 1.645 (0.10)\right] [1.05]}{1.66} = 0.528 E_{app}$$

where: $E_{min} = E_{x min}$, $E_{y min}$, or $E_{axial min}$ as appropriate $E_{app} = E_{x app}$, $E_{y app}$, or 0.95 E_{axial} as appropriate $CoV_F = \text{coefficient of variation for modulus of elasticity}$

2.6 Tension Parallel to Grain Design Value, F_t

A single design value is tabulated for tension parallel to grain for each combination or stress class.

2.7 Compression Parallel to Grain Design Value, F_c

A single design value is tabulated for compression parallel to grain for each optimized combination or stress class. Uniform grade combinations have separate values tabulated for members with 2 or 3 laminations and for members with 4 or more laminations.

2.8 Radial Compression Design Values, F_{rc}

The design value for radial compression, F_{rc} , shall be equal to the design value for compression perpendicular to grain of the side faces, $F_{c\perp v}$.

2.9 Radial Tension Design Values, F_{rt}

For southern pine, the design value for radial tension (tension perpendicular to the longitudinal axis of a curved member), F_{rt} , shall be equal to 1/3 of the shear design value, F_{vx} , for non-prismatic members. Radial reinforcement shall not be required.

For all other softwood species, the reference design value for radial tension shall be limited to 15 psi (100 kPa) for loads other than wind or earthquake loads. If the calculated radial tension stress (due to loads or load combinations not including wind or seismic loads) exceeds 15 psi (100 kPa) multiplied by appropriate adjustment factors, radial reinforcement shall be required. Design values for radial tension for radially-reinforced members shall be limited to 1/3 of the shear design value for non-prismatic members. Radial reinforcement shall be designed in accordance with the Timber Construction Manual (2). For wind and earthquake loading, the design value for radial tension shall be 1/3 of the shear design value for non-prismatic members.

Loading type	Softwood Species Other Than Southern Pine	Southern Pine
Wind or seismic	1/3 of F _{vx} for non-prismatic members	1/3 of F _{vx} for non-prismatic member
Other loading	15 psi ^(a)	1/3 of F _{vx} for non-prismatic member

(100 kPa) multiplied by appropriate adjustment factors, radial reinforcement shall be required. Design values for radial tension fo radially-reinforced members shall be limited to 1/3 of the shear design value for non-prismatic members. Radial reinforcement shall be designed in accordance with the Timber Construction Manual (2).

2.10 Torsion Design Values, F_{vt}

The torsion design value shall be taken as 2/3 of the shear design value, F_{vx} , for non-prismatic members.

2.11 Modulus of Rigidity

In lieu of specific data, the modulus of rigidity shall be taken as 1/16 of the long-span modulus of elasticity, as defined in the ASTM D3737 (9), or E_{true} for the lowest grade lamination used in the lay-up. If data are available, they shall be permitted to be used to determine the modulus of rigidity.

Note: The lowest grade lamination used in the lay-up can be found in *Annex B*. The E_{true} for the lowest grade lamination can be determined from *Table A2* based on $E_{true} = E_{axial}$, as specified in Section 2.5.

2.12 Reference Design Value Tables

The design values in *Table A1* and *Table A1-Expanded* are applicable to members with 4 or more laminations and are intended primarily for members stressed in bending about the x-x axis (Figure 2.1-1). Design values are included, however, for axial stresses and stresses from bending about the y-y axis (Figure 2.1-1). The values in *Table A1* are for the industry recommended stress classes. Each stress class is representative of a group of combinations with similar design values. Design values for individual combinations are shown in *Table A1-Expanded*.

Table A2 contains design values for timbers with uniform grade lay-ups. These combinations are intended primarily for timbers loaded axially or in bending about the y-y axis (Figure 2.1-1). Design values are included, however, for bending about the x-x axis (Figure 2.1-1).

The design values in *Table A3* are applicable to stress classes and combinations that have been modified by secondary manufacturing or fabrication by removing material from the compression face to create a tapered beam. The design values in *Table A3* shall replace the corresponding design values in *Table A1* or *Table A1-Expanded* for all such tapered beams. For members manufactured with taper in the laminating plant with compression zone grade requirements maintained, the design values published in *Table A1* shall apply.

3. LAY-UP REQUIREMENTS

3.1 Lumber Grades

Lumber grades shall be in accordance with *Annex C* of this standard and Section 4.3—*Lumber for Laminating* of ANSI A190.1 (3).

3.2 Substitutions

Lumber of higher grades of the same species is permitted to be substituted in all lay-ups with some restrictions. Visually graded lumber shall not be permitted to be substituted for E-rated lumber. Substitutions of E-rated lumber grades for visual grades of lumber shall be approved by the laminator's accredited inspection agency prior to making the substitution. Full or partial length substitutions are permitted.

3.3 Determining Number of Laminations in Each Zone

The number of laminations to use in each zone in the lay-up shall be calculated based on the percentages shown in *Tables B1 and B2*. Percent values shall be multiplied by the total depth of the member expressed in the number of laminations. The required number of laminations shall be determined starting with the outer zones and working inward. When the calculated number of laminations results in a fractional number, the fractional number of laminations shall be rounded upward to the next whole number. For the inner zones, the resulting excess of percentage resulting from rounding upward of the outer zone is permitted to be subtracted from the next inner zone requirements.

Example: The tension zone of a hypothetical 16 lamination beam requires 5% 302-24, 15% L1, and 10% L2.

The number of 302-24 laminations is determined by: $16 \times 0.05 = 0.8$ (rounded up to 1).

The combined number of 302-24 and L1 laminations is: $16 \times (0.05 + 0.15) = 3.2$ lams (round up to 4). Since there is already 1 lam of 302-24 from the calculation above, the required number of L1 lams is 4 - 1 = 3 lams.

The combined number of 302-24, L1, and L2 lams is $16 \times (0.05 + 0.15 + 0.10) = 4.8$ lams (rounded up to 5). Since there are already 1 lam of 302-24 and 3 lams of L1 from the calculation above, the required number of L2 lams is 5 - 4 = 1 lam.

Where more than one thickness is used within a member and those lamination thicknesses vary by more than 3/16 inch, the total thickness of each grade of lumber required in the inner and outer tension and compression zones shall be determined by using the thickness lamination in the member as the basic lamination thickness.

Example: When the thickest lamination used is 1-3/8 inches (35 mm) and 1.6 inches (41 mm) of L1 grade is required in a zone (based on multiplying the percentage required for that zone in the table by the depth of the member in inches), then a total thickness of at least 2-3/4 inches (70 mm) of L1 grade is required in that zone.

3.4 Wane

Certain combinations are permitted to contain wane. These combinations are for dry conditions of use only, except as allowed in ANSI A190.1 (3). These combinations allow wane up to 1/6 the width of the member on each side of the member. When this is the case, the basic shear design value shall be reduced by 1/3. When wane is restricted to just one side of the member, the basic design shear value shall be reduced by 1/6. When wane material is used in these combinations, members shall be for industrial or framing appearance grades and for prismatic members only.

Selectively placed wane is permitted for use in glued laminated timber combinations without a corresponding reduction in shear design values based on the following set of rules. Combinations meeting these requirements are for dry conditions of use only, except as allowed in ANSI A190.1 (3). When wane material is used in these combinations, members shall be for industrial or framing appearance grades and for prismatic members only.

- 1. Lumber with wane up to 1/6 of the finished member width and 1/2 of the lamination thickness shall be permitted on only one side of the member.
- 2. No wane shall be permitted within the central 40% of the depth of the cross section.
- 3. No wane shall be permitted in the outer laminations (top and bottom).
- 4. No wane shall be permitted in the 302 grade tension laminations.
- 5. No wane shall be permitted at the glue lines adjacent to the top or bottom laminations or at glue lines adjacent to 302 grade tension laminations.
- 6. Wane shall not be permitted at the interior edge joint of multi-piece laminations.
- 7. Combinations utilizing wane conforming to these rules shall be designated with a "W1" in the combination symbol (i.e., 24F-V1-W1). Appropriate stamps shall be obtained from the laminator's accredited inspection agency prior to production.

3.5 Tension Laminations

3.5.1 General

The flexural design values for most combinations listed in *Table A1* require the use of specially graded tension laminations in the outer 5% of beam depth on the tension side(s). These special grades are designated as "302 tension laminations" and commonly referred to as "special tension laminations."

3.5.2 Combinations without 302 Tension Laminations

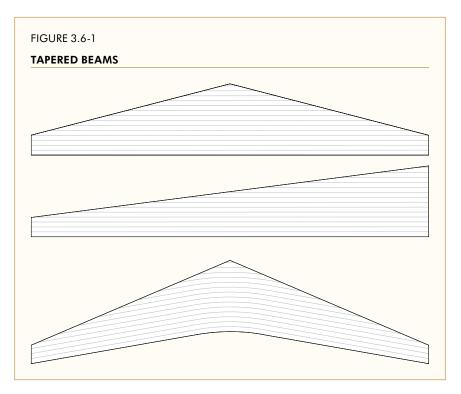
Combinations requiring 302 tension laminations are permitted to be manufactured without the 302 tension lamination grade requirements provided the tabular design value for extreme fiber in bending about the x-x axis, F_{bx} , is multiplied by 0.75 for depths greater than 15 inches (380 mm) or by 0.85 for depths less than or equal to 15 inches (380 mm). When the 302 tension laminations specified in *Table B1* are omitted in visually graded lay-ups that normally require 302 tension laminations, they shall be replaced by dense laminations with a maximum slope of grain of 1:14 with knots and other strength-reducing characteristics meeting the requirements of L1 or No. 1, based on the normal lamination grading requirements used for the species.

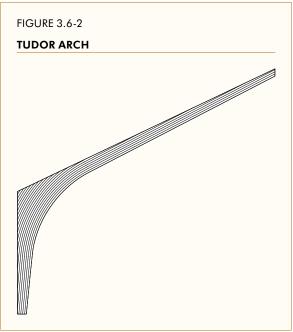
3.5.3 Arches

302 tension laminations shall not be required for arches.

3.6 Tapered Members

Combination requirements, including 302 tension lamination requirements, shall apply for every cross-section along the entire length of tapered beams (Figure 3.6-1) unless the shop drawings or instructions from the designer indicate otherwise. Tudor arches (Figure 3.6-2) shall be laid up in accordance with AITC/WCLIB 200 (1) or APA Quality Assurance Policy for Structural Glued Laminated Timber (5), unless specified otherwise.





3.7 Fire-Resistive Construction

When bending members are specified to be one-hour fire-resistive, they shall be manufactured to the specified lay-up as tabulated except that a core lamination shall be removed, the tension zone moved inward and the equivalent of one additional nominal 2-inch thickness outer tension lamination added.

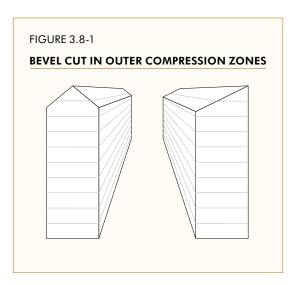
When bending members are specified to be one-and-one-half-hour or two-hour fire-resistive, they shall be manufactured to the same lay-up as tabulated except that two core laminations shall be removed, the tension zone moved inward and the equivalent of two additional nominal 2-inch thickness outer tension laminations added.

For members designed for fire exposure on four sides, both the top and bottom of the lay-up shall be modified to meet these requirements. For lay-ups designed for fire exposure on three sides, only the bottom shall require modification.

Lay-ups modified to meet these requirements shall be marked with "1-HOUR FIRE RATING" if one additional tension lamination is used or "2-HOUR FIRE RATING" if two additional tension laminations are used. Additionally, balanced lay-ups designed and manufactured for three-sided fire exposure shall be marked with "TOP" on the appropriate face to ensure proper orientation in the structure.

3.8 Cross Sections with Bevel Cuts on Compression Face

Beams manufactured with a bevel cut (or cuts) on the compression face (Figure 3.8-1) shall be laid up so that the grade of laminations in the outer compression zone is maintained through the entire depth of the bevel cut. Where necessary, core laminations shall be removed and additional compression laminations shall be added to meet this requirement.



3.9 Non-Standard Depths

For beams with non-standard depths, (i.e., I-joist compatible depths, etc.), grade requirements of the combination shall be maintained throughout the depth of the lay-up.

For unbalanced lay-ups, any of three options shall be permitted to be used:

- (1) All laminations are permitted to be planed to a constant thickness.
- (2) One or more core laminations are permitted to be planed to a thinner dimension.
- (3) A core lamination is permitted to be removed with one extra compression lamination added with the excess material removed from the compression side after laminating.

For balanced lay-ups, either Option (1) or Option (2) shall be used.

4. ALTERNATE COMBINATIONS

4.1 General

The development and use of alternate combinations allows for more efficient and innovative use of the lumber resource. Combinations not listed in this Specification shall be permitted to be used, subject to the provisions of this Section.

Alternate lay-ups shall be approved by the laminator's accredited inspection agency prior to production. Alternate combinations shall be given a unique designation following industry protocols for assigning combination symbols.

4.2 Design Values

Design values for alternate lay-ups shall be established by analysis in accordance with ASTM D3737 (9) or by full-scale testing in accordance with ASTM D7341 (13) and analysis in accordance with ASTM D2915 (8). All design values shall be approved by the laminator's accredited inspection agency before use.

4.2.1 Design Values by Analysis Only

For combinations developed by analysis only, the design values shall be established according to ASTM D3737 (9). In addition, for horizontally laminated beams, the maximum outer fiber bending stress calculated according to transformed section analysis shall not exceed the nominal bending stress by more than 10% unless the end joints are qualified and maintained at a higher qualification stress level (QSL).

4.2.2 Design Values by Full-Scale Testing and Analysis

Design values shall be permitted to be established following the procedures of ASTM D7341 (13) and ASTM D2915 (8). Samples chosen for full-scale testing shall be representative of production. Full scale beam tests shall be conducted by an accredited testing lab or witnessed by a representative of an accredited inspection agency.

4.3 Quality Assurance

The production parameters and end joint QSL's from the initial qualification shall be the basis of the manufacturing facility's quality assurance requirements for alternate lay-ups with design values established by full-scale testing. Documentation of these requirements shall be maintained at the manufacturing facility and shall be available to the laminator's accredited inspection agency. Periodic evaluation shall be conducted as required by ASTM D7341 (13) to ensure that test-based design values are maintained over time.

4.4 Documentation

Documentation of the design values and lay-up requirements for alternate lay-ups shall be maintained by the accredited inspection agency and by the laminator. This documentation shall be available to the public upon request.

ANNEX A DESIGN VALUE TABLES FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER

TABLE A1

REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER

(Members stressed primarily in bending) (Tabulated design values are for normal load duration and dry service conditions.)

					1			1
			Fasteners	Specific Gravity for Fastener Design	O	0.41 0.41 0.42	0.50(1)	0.50(i) 0.55 0.55
			Axially Loaded	Com- pression Parallel to Grain	F _c (psi)	925 925 1000	1600	1600 1750 1750
			Axially	Tension Parallel to Grain	F _t (psi)	675 725 775	1100	1150 1250 1250
			sticity	For Stability Calcu- lations	E _{y min} 10 ⁶ psi)	0.58 0.63 0.69	0.85	0.85 0.90 0.90
	minations		Modulus of Elasticity	For Deflection Calculations	E _{y app} (10 ⁶ psi)	1.1	1.6	1.6 7.1 7.1
,	Y-Y Axis aces of La		Modu	Fe Defle Calcul	Eytrue (10 ⁶ psi)	1.3	1.7	1.7
	Bending About Y-Y Axis rallel to Wide Faces of Lo			Shear Parallel to Grain	F _{vy} (e) (psi)	170 170 185	230(c)	230 ^(c) 260 260
	Bending About Y-Y Axis Loaded Parallel to Wide Faces of Laminations			Extreme Compression Fiber in Perpendicular Bending to Grain	F _{cLy} (psi)	315 315 315	260	560 650 650
5	_			Extreme Fiber in Bending	F _{by} (psi)	800 800 1050	1450	1600 1600 1750
			sticity	For Stability Calcu- Iations	E _{x min} (106 psi)	0.69 0.79 0.90	0.95	1.00
	ons		Modulus of Elasticity	For Deflection Calculations	Е _{х арр} (10 ⁶ psi)	1.3 1.5 1.7	1.8	1.9 2.10 2.10
	f Laminati		Modu	P. Defle Calcul	E _{x true} (10 ⁶ psi)	1.6 1.8 1.8	1.9	2.2 ⁽¹⁾ 2.2 ⁽¹⁾ 2.2 ⁽¹⁾
	out X-X Axis Wide Faces of Laminations			Shear Parallel to Grain	F _{vx} (d) (psi)	195 195(f) 210(f)	265(c)	265 ^(c) 300 300
	Bending About X-X Axis Loaded Perpendicular to Wide Faces o			Compression Perpendicular to Grain	F _{c.t.x} (psi)	315 425 500	929	650 805 805
	Loaded Perp	Extreme Fiber in Bending	Top	ot Beam Stressed in Tension (Negative Bending)	F _{bx} -(a) (psi)	925 1100 1450	1450(b)	1950 2300 2400
		Extreme Fibe	Bottom	of Beam Stressed in Tension (Positive Bending)	F _{bx} + (psi)	1600 2000 2400	2400	2600 2800 3000
					Stress Class	16F-1.3E 20F-1.5E 24F-1.7E	24F-1.8E	26F-1.9E(a) 28F-2.1E SP(a) 30F-2.1E SP(a)(h)

Footnotes to Table A1

- For balanced layups, F_{bx} shall be equal to F_{bx} + for the stress class. Designer shall specify when balanced layup is required
- Negative bending stress, F_{bx} is permitted to be increased to 1850 psi for Douglas-Fir and to 1950 psi for southern pine for specific combinations. Designer shall specify when these increased stresses are required.
- For structural glued laminated timber of southern pine, the basic shear design values, F_{∞} and F_{∞} , are permitted to be increased to 300 psi and 260 psi, respectively.
- e design values for shear, F., and F., shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall also be used for determination of design values for radial tension and torsion. (a) For I (b) Neg (c) For s (d) The c
- €

Design values are for timbers with laminations made from a single piece of lumber across the width or multiple pieces that have been edge bonded. For timbers manufactured from multiple piece of lumber across the width or are not edge bonded, value shall be multiplied by 0.4 for members with 5, 7, or 9 laminations or by 0.5 for all other members. This reduction shall be cumulative with the adjustment in footnote (d).

- Certain southern pine combinations may contain lumber with wane. If lumber with wane is used, the design value for shear parallel to grain, F.w. shall be multiplied by 0.67 if wane is allowed on both sides. If wane is limited to one side, F.w. shall be multiplied by 0.83. This reduction shall be cumulative with the adjustment in footnote (d).
 - combinations are restricted to a maximum 6 in. nominal width unless the manufacturer has qualified for wider widths based on full-scale tests subject to approval by an accredited inspection agency (g) 26F, 28F, and 30F beams are not produced by all manufacturers, therefore, availability may be limited. Contact supplier or manufacturer for details. (h) 30F
- For 28F and 30F members with more than 15 laminations, $E_{xtrue} = 2.1 \times 10^6$ psi and $E_{x\,app} = 2.0 \times 10^6$ psi.

(i) For structural glued laminated timber of southern pine, specific gravity for fastener design is permitted to be increased to 0.55.

Stress classes represent groups of similar glued laminated timber combinations. Values for individual combinations are included in Table A1-Expanded. Design values are for members with 4 or more laminations. For 2 and 3 lamination members, see Table A2. Some stress classes are not available in all species. Contact manufacturer for availability.

(e)

TABLE A1-EXPANDED

REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER COMBINATIONS^(a) (Members stressed primarily in bending) (Tabulated design values are for normal load duration and dry service conditions.)

																	Т.		
	Fasteners	Gravity or r Desig	Side Face	ტ	.41	0.50	0.50 0.50 0.43	0.55	0.55 0.55 0.55	.41	0.50	0.46	0.46	0.50	0.43 0.41 0.42 0.42	0.55 0.55 0.55 0.55	.42	0.43 0.43 0.43	0.55 0.43 0.55
	Faste	Specific Gravity for Fastener Design	Top or Bottom Face		0.	0.50 0.50 0.43	0.50 0.50 0.43	0.55	0.55 0.55 0.55	0.	0.50	0.46	0.46	0.50	0.43 0.41 0.42	0.55 0.55 0.55 0.55	3	0.50 0.50 0.43 0.43	0.55 0.55 0.55
	Loaded		Com- pression Parallel to Grain	F _c (psi)	925	1500 1600 1150	1600 1600 1250	1300	1550 1550 1550	925	1550	1550	1600	1600	1450 1100 2000 1750	1400 1400 1500 1550	1000	1450 1550 1550 1500	1500 1350 1600
	Axially Loaded		Tension Parallel to Grain	F _† (psi)	675	975 1000 825	975 1000 875	1000	1000	725	1000	950 900	900	1050	1050 825 1150 900	1000 1000 1050 1050	775	1100 1150 1150 975	1100 975 1150
	s)		iticity	E _{y min} (10 ⁶ psi)	0.58	0.79	0.79 0.79 0.74	0.74	0.79 0.85 0.85	0.63	0.79	0.74	0.74	0.85	0.74 0.74 0.85 0.79	0.74 0.79 0.74 0.85	69.0	0.79 0.79 0.79 0.79	0.79 0.79 0.85
	mination		Modulus of Elasticity	Eyapp (10 ⁶ psi)	1.1		 5 5	4.1	5. 6. 6.	1.2	1.5	 i 4 4	4 4	1.6	4. 4. 6. ci	4. 7. 4. 6. 4	 E.	2: L 2: L 3: C	5: L 6: L
About Y.Y Axis	aces of La		ПроМ	Ey true (10 ⁶ psi)	1.2	6 6 4	6 6 4 6 4	 	1.7.	1.3	1.6	ـــــــــــــــــــــــــــــــــــــ	. r. r.	1.7	5: L 5: L 6: L	3: L 3: L 5: L	1.4	6 6 6 6	3.1.6
	to Wide F		Shear Parallel to Grain	F _{vy} (c) (psi)	170	230 230 190	230 230 190	260	260 260 260	170	230	230	230	230	190 175 190 195	260 260 260 260	185	200 200 190 190	260 230 260
	(Loaded Parallel to Wide Faces of Laminations)		Compression Perpendicular to Grain	F _{c⊥y} (psi)	315	560 560 375	560 560 375	650	650 650 650	315	560	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	470 375	560 560	375 315 470 470	650 650 650 650	315	375 375 375 375	650 470 650
5	(Lo		Extreme Fiber in Bending	F _{by} (psi)	800	1450 1450 1200	1400 1550 1350	1450	1600 1400 1650	800	1450	1250	1300	1400 1550	1450 1000 1150 1200	1450 1600 1450 1400	1050	1350 1450 1550 1200	1450 1350 1700
5			sticity	E _{x min} (10 ⁶ psi)	69.0	0.79	0.85 0.85 0.74	0.79	0.85 0.85 0.90	0.79	0.85	0.79	0.79	0.90	0.85 0.79 0.85 0.85	0.79	06:0	0.90 0.95 0.95 0.95	0.90
5	tions)		Modulus of Elasticity	E _{x app} (10 ⁶ psi)	1.3	1.5 1.6 4.1	1.6 1.4	1.5	1.6 1.7 7.1	1.5	1.6	 	5.1	1.7	1.6 1.5 1.6	1.5	1.7	7.7 1.8 1.8 1.8	1.7
5	Wide Faces of Laminations		Modow	E _{x true} (10 ⁶ psi)	1.4	1.6	1.7 1.5	1.6	1.7	1.6	1.7	9 7 7	9.1	8. 6.	1.8 1.6 7.1 7.1	6. L. L. S.	8.	1.9	8. 6. 6.
hout X-X Axis	de Faces		Shear Parallel to Grain	F _{vx} (b) (psi)	195	265 265 215	265 265 215	300	300	195	265 265	265 265 265	265 215	265 265	215 200 215 215	300	210	215 215 215 215	300 210 300
- 1 -	lar to Wi	Compression Perpendicular to Grain	Com- pression Face	F _{c⊥x} (psi)	315	560 560 375	560 560 375	650	650 650 650	425	560	280 280 280	200	560 560	500 450 560 650	650 650 740 650	200	650 650 500 500	650 650 740
Renc	erpendic	Compr Perpen to G	Tension Face	ج <u>م</u>	31	560 560 375	560 560 375	740	650 650 650	42	650	260 560 560	260 560 500	560 560	500 450 560 560	740 650 740 650		650 650 500 500	740 740 740
	(Loaded Perpendicular to	xtreme Fiber in Bending	Top of Beam Stressed in Tension (Negative Bending)	F _{bx} - (psi)	925	1250 1600 1050	1200 1600 1600	1400	1600 1250 1600	1100	1450 2000	2000	2000	1200 2000	2000 1300 2400 1550	1550 1450 2000 1300	1450	1600 2400 2400 1600	1750 1650 2400
		Extreme Fiber in Bending	Bottom of beam Stressed in Tension (Positive Bending)	F _{bx} + (psi)	1600	1600	1600 1600 1600	1600	1600 1600 1600	2000	2000	2000	2000	2000 2000	2000 2000 2400 2400	2000 2000 2000 2000	2400	2400 2400 2400 2400	2400 2400 2400
			2000	Outer/ Core	1.3E	DF/DF DF/DF HF/HF	DF/DF DF/DF HF/HF	SP/SP SP/SP	SP/SP SP/SP SP/SP	1.5E					HF/HF ES/ES SPF/SPF SPF/SPF	SP/SP SP/SP SP/SP SP/SP	1.7E	DF/HF DF/HF HF/HF HF/HF	SP/SP SP/SP SP/SP
				nation Symbol	16F-1.3E	16F-V3 16F-V6 16F-E2	16F-E3 16F-E6 16F-E7	16F-V2 16F-V3	16F-V5 16F-E1 16F-E3	20F-1.5E	20F-V3 20F-V7	20F-V13	20F-V15 20F-E2	20F-E3 20F-E6	20F-E7 20F-E8 24F-E/SPF1 24F-E/SPF3	20F-V2 20F-V3 20F-V5 20F-E1	24F-1.7E	24F-V5 24F-V10 24F-E11 24F-E15	24F-V1 24F-V4 ^(d) 24F-V5

TABLE A1-EXPANDED (Continued)

REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER COMBINATIONS(a)

(Members stressed primarily in bending) (Tabulated design values are for normal load duration and dry service conditions.)

Footnotes to Table A1-Expanded:

- (a) The combinations in this table are applicable to members consisting of 4 or more laminations and are intended primarily for members stressed in bending due to loads applicable to members consisting of 4 or more laminations and faces of the laminations. For combinations and design values are tabulated for loading both perpendicular and parallel to the wide faces of the laminations, see Table 42. For members of 2 or 3 laminations, see Table 42.
- The design values for shear, F_{ex} and F_{ex} shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall also be used for determination of design values for radial tension and torsion. Design values are for timbers with laminations made from a single piece of lumber across the width or multiple pieces that have been edge bonded. For timber manufactured from multiple piece laminations not edge-bonded, value shall be cumulative with the adjustment in footnote (b). **(**9) Û
 - This combination may contain lumber with wane. If lumber with wane is used, the design value for shear parallel to grain, F., shall be multiplied by 0.67 if wane is allowed on both sides. If wane is limited to one side, F., shall be multiplied by 0.83. This reduction shall be cumulative with the adjustment in footnote (b). <u>(</u>
- 26f, 28F, and 30F beams are not produced by all manufacturers; therefore, availability may be limited. Contact supplier or manufacturer for details. 30F combinations are restricted to a maximum 6 in. nominal width unless the manufacturer has qualified for wider widths based on full-scale tests sub
- combinations are restricted to a maximum 6 in. nominal width unless the manufacturer has qualified for wider widths based on full-scale tests subject to approval by an accredited inspection agency.
 - For 28F and 30F members with more than 15 laminations, $E_{x\,true} = 2.1 \times 10^6$ psi, $E_{x\,capp} = 2.0 \times 10^6$ psi, and $E_{x\,min} = 1.06 \times 10^6$ psi.

TABLE A2

REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER (Members stressed primarily in axial tension or compression)

(Tabulated design values are for normal load duration and dry service conditions.)

				All Lo	ading		Ax	ially Load	led	-				X-X	g About Axis ded
											ending ab d Parallel Lamin			Perpen to Wide	dicular Faces of ations
			Modu	ilus of Ela	sticity		Tension Parallel to Grain	Compr Parallel	ession to Grain		Bending		Shear Parallel to Grain (a)(b)(c)	Bending	Shear Parallel to Grain ^(c)
Combi- nation Symbol	Species	Grade	E _{axial} (10 ⁶ psi)	0.95 E _{axial} (10 ⁶ psi)	E _{axial min}	Com- pression Perpen- dicular to Grain F _{cL} (psi)	2 or More Lami- nations F _t (psi)	4 or More Lami- nations F _c (psi)	2 or 3 Lami- nations F _c (psi)	4 or More Lami- nations F _{by} (psi)	3 Lami- nations F _{by} (psi)	2 Lami- nations F _{by} (psi)	F _{vy} (psi)	2 Laminations to 15 in. Deep ^(d) F _{bx} (psi)	F _{vx} (psi)
Visually	Graded	Western	Species												
1 2 3 4 5	DF DF DF DF DF	L3 L2 L2D L1CL L1	1.6 1.7 2.0 2.0 2.1	1.5 1.6 1.9 1.9 2.0	0.79 0.85 1.00 1.00 1.06	560 560 650 590 650	950 1250 1450 1400 1650	1550 1950 2300 2100 2400	1250 1600 1900 1950 2100	1450 1800 2100 2200 2400	1250 1600 1850 2000 2100	1000 1300 1550 1650 1800	230 230 230 230 230 230	1250 1700 2000 2100 2200	265 265 265 265 265 265
14 15 16 17	HF HF HF	L3 L2 L1 L1D	1.4 1.5 1.7 1.8	1.3 1.4 1.6 1.7	0.69 0.74 0.85 0.90	375 375 375 500	800 1050 1200 1400	1100 1350 1500 1750	1050 1350 1500 1750	1200 1500 1750 2000	1050 1350 1550 1850	850 1100 1300 1550	190 190 190 190	1100 1450 1600 1900	215 215 215 215 215
22 ^(e)	SW	L3	1.1	1.0	0.53	315	525	850	725	800	700	575	170	725	195
69 70 71 72	AC AC AC AC	L3 L2 L1D L1S	1.3 1.4 1.7 1.7	1.2 1.3 1.6 1.6	0.63 0.69 0.85 0.85	470 470 560 560	725 975 1250 1250	1150 1450 1900 1900	1100 1450 1900 1900	1100 1400 1850 1850	975 1250 1650 1650	775 1000 1400 1400	230 230 230 230	1000 1350 1750 1900	265 265 265 265
73 74 75	POC POC POC	L3 L2 L1D	1.4 1.5 1.8	1.3 1.4 1.7	0.69 0.74 0.90	470 470 560	775 1050 1350	1500 1900 2300	1200 1550 2050	1200 1450 1950	1050 1300 1750	825 1100 1500	230 230 230	1050 1400 1850	265 265 265
Visually	Graded	Southerr	n Pine												
47 47 1:10 47 1:8 48 48 1:10 48 1:8 49 49 1:14 49 1:12 49 1:10 50 50 1:12 50 1:10	SP SP SP SP SP SP SP SP SP SP	N2M12 N2M10 N2M N2D12 N2D10 N2D N1M16 N1M14 N1M12 N1M N1D14 N1D14 N1D12	1.5 1.5 1.5 1.8 1.8 1.8 1.8 1.8 2.0 2.0	1.4 1.4 1.4 1.7 1.7 1.7 1.7 1.7 1.7 1.9 1.9	0.74 0.74 0.74 0.90 0.90 0.90 0.90 0.90 0.90 0.90 1.00	650 650 650 740 740 740 650 650 650 650 740 740	1200 1150 1000 1400 1350 1350 1350 1350 1550 1500 1350	1900 1700 1500 2200 2000 1750 2100 2000 1900 1700 2300 2300 2200 2000	1150 1150 1150 1350 1350 1350 1450 1450 1450 1450 1700 1700	1750 1750 1600 2000 2000 1850 1950 1950 1950 1850 2300 2300 2100	1550 1550 1550 1800 1800 1800 1750 1750 1750 1750 2100 2100	1300 1300 1300 1500 1500 1500 1500 1500	260 260 260 260 260 260 260 260 260 260	1400 1400 1400 1600 1600 1600 1800 1800 1800 2100 2100 2100	300 300 300 300 300 300 300 300 300 300

Footnotes to Table A2

- (a) For members with 2 or 3 laminations, the shear design value for transverse loads parallel to the wide faces of the laminations, F_{vyr} shall be reduced by multiplying by a factor of 0.84 or 0.95, respectively.
- (b) The shear design value for transverse loads applied parallel to the wide faces of the laminations, F_{vv}, shall be multiplied by 0.4 for members with 5, 7, or 9 laminations manufactured from multiple piece laminations (across width) that are not edge bonded. The shear design value, F_{vv}, shall be multiplied by 0.5 for all other members manufactured from multiple piece laminations with unbonded edge joints. This reduction shall be cumulative with the adjustment in footnotes (a) and (c).
- (c) The design values for shear, F_{vx} and F_{vy} , shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall be used for design of members at connections that transfer shear by mechanical fasteners. The reduced design value shall also be used for determination of design values for radial tension and torsion.
- (d) The tabulated F_{bx} values are for members without special tension lams up to 15 inches in depth. If the member depth is greater than 15 inches without special tension lams, the tabulated F_{bx} values must be multiplied by a factor of 0.88. If special tension lams are used, the tabulated F_{bx} values are permitted to be increased by a factor of 1.18 regardless of the member depth.
- (e) When Western Cedars, Western Cedars (North), Western Woods, and Redwood (open grain) are used in combinations for Softwood Species (SW), the design value for modulus of elasticity shall be reduced by 100,000 psi. When Coast Sitka Spruce, Coast Species, Western White Pine, and Eastern White Pine are used in combinations for Softwood Species (SW) tabulated design values for shear parallel to grain, F_{vx} and F_{vyr} shall be reduced by 10 psi, before applying any other adjustments.

TABLE A3

REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED

SOFTWOOD TIMBER COMBINATIONS WITH TAPER CUTS (FIGURE 3.6-1) ON THE COMPRESSION FACE(a)(b)

	(psi)	(10 ⁶ psi)	(10 ⁶ psi)	E _{x min} (10 ⁶ psi)	(psi)	(psi)
1.3E	1050	1.3	1.2	0.63	315	140
DF/DF	1600	1.6	1.5	0.79	560	190
DF/DF	1600	1.6	1.5	0.79	560	190
HF/HF						155
DF/DF	1600					190
DF/DF	1600	1.7	1.6	0.85	560	190
HF/HF	1350	1.5	1.4	0.74	375	155
SP/SP	1450	1.6	1.5	0.79	650	215
SP/SP			1.4	0.74		215
						215
	1600	1.7				215
SP/SP	1600	1.7	1.6	0.85	650	215
1.5E	1250	1.5	1.4	0.74	375	150
DF/DF	1900			0.85	560	190
						190
	1650					190
						190
	1700				375	155
	1900					190
					560	190
						155
						215
						215
	1050		1.5			215 215
3F/3F SP/SP	1930					215
						150
DE/HE						190
						155
						155
						155
						155
SP/SP	1800			0.85	650	215
SP/SP	1250	1.5	1.4	0.74	470	215
SP/SP	2100	1.8	1.7	0.90	650	215
1.8E	2000	1.8	1.7	0.90	560	190
DF/DF	2100	1.8	1.7	0.90	560	190
DF/DF	2100	1.8	1.7	0.90	560	190
DF/DF	2100	1.8	1.7	0.90	560	190
	2100	1.8				190
				0.90		190
		1.8	1.7			215
						215
						215 215
						190
						190
						190
						215
						215
						215
SP/SP	2000	1.9		0.95	650	215
SP/SP	2000	1.9	1.8	0.95	740	215
2.1E	2400	2.0	1.9	1.00	650	215
SP/SP	2400	2.0	1.9	1.00	650	215
						215
						215
SP/SP	2400	2.0	1.9	1.00	650	215
	DF/DF DF/DF HF/HF DF/DF HF/HF DF/DF HF/HF SP/SP	DF/DF 1600 DF/DF 1600 HF/HF 1350 DF/DF 1600 DF/DF 1600 DF/DF 1600 HF/HF 1350 SP/SP 1450 SP/SP 1450 SP/SP 1550 SP/SP 1550 SP/SP 1600 DF/DF 1900 DF/DF 1900 AC/AC 1650 AC/AC 1650 AC/AC 1650 HF/HF 1700 DF/DF 1900 SP/SP 1500 SP/SP 1500 SP/SP 1500 SP/SP 1500 SP/SP 1500 SP/SP 1500 SP/SP 1950 SP/SP 1950 SP/SP 1950 SP/SP 1950 DF/DF 1900 SP/SP 1900	DF/DF 1600 1.6 DF/DF 1600 1.6 HF/HF 1350 1.5 DF/DF 1600 1.7 DF/DF 1600 1.7 DF/DF 1600 1.7 DF/DF 1600 1.7 HF/HF 1350 1.5 SP/SP 1550 1.6 SP/SP 1550 1.5 SP/SP 1550 1.6 SP/SP 1600 1.7 SP/SP 1600 1.7 SP/SP 1600 1.7 DF/DF 1900 1.7 DF/DF 1900 1.7 DF/DF 1900 1.7 AC/AC 1650 1.5 AC/AC 1650 1.5 HF/HF 1700 1.6 DF/DF 1900 1.7 DF/HF 1700 1.6 SP/SP 1500 1.5 SP/SP 1500 1.5 SP/SP 1500 1.5 SP/SP 1500 1.6 SP/SP 1500 1.7 SP/SP 1500 1.7 SP/SP 1900 1.7 DF/HF 1900 1.7 DF/HF 1900 1.7 SP/SP 1900 1.7 SP/SP 1950 1.7 SP/SP 1950 1.7 SP/SP 1900 1.8 SP/SP 2100 1.8 DF/DF 2100 1.8 DF/DF 2100 1.8 SP/SP 2100 1.9 SP/SP 2000 2.0 SP/SP 2000 2.0 SP/SP 2000 2.0 SP/SP 2000 2.0	DF/DF 1600 1.6 1.5 1.5 1.4 DF/DF 1600 1.6 1.5 1.4 DF/DF 1600 1.7 1.6 DF/DF 1600 1.7 1.6 DF/DF 1600 1.7 1.6 DF/DF 1600 1.7 1.6 I.5 SP/SP 1450 1.6 1.5 SP/SP 1450 1.6 1.5 SP/SP 1550 1.5 1.4 SP/SP 1550 1.5 1.4 SP/SP 1550 1.5 1.4 SP/SP 1600 1.7 1.6 SP/SP 1700 1.5 1.4 SP/SP 1700 1.6 1.5 SP/SP 1700 1.6 SP/SP 1500 1.5 SP/SP 1500 1.5 SP/SP 1500 1.5 SP/SP 1500 1.5 SP/SP 1500 1.6 SP/SP 1700 1.7 1.6 SP/SP 1700 1.6 SP/SP 1700 1.6 SP/SP 1700 1.7 1.6 SP/SP 1800 1.7 1.8 SP/SP 1800 1.9 1.8 SP/SP 1800 1.9 1.8 SP/SP 1800 1.9 1.8 SP/SP 1800 1.9 1.8	DF/DF 1600 1.6 1.5 0.79 DF/DF 1600 1.6 1.5 0.79 DF/DF 1600 1.6 1.5 0.79 DF/DF 1600 1.7 1.6 0.85 DF/DF 1600 1.7 1.6 0.85 DF/DF 1600 1.7 1.6 0.85 DF/DF 1500 1.5 1.4 0.74 SP/SP 1550 1.5 1.4 0.74 SP/SP 1550 1.6 1.5 0.79 SP/SP 1600 1.7 1.6 0.85 SP/SP 1900 1.7 1.6 0.85 SP/SP 1900 1.7 1.6 0.85 AC/AC 1650 1.5 1.4 0.74 HF/HF 1700 1.6 1.5 0.79 DF/DF 1900 1.7 1.6 0.85 SP/SP 1500 1.5 1.4 0.74 SP/SP 1500 1.5 1.4 0.74 SP/SP 1500 1.5 1.4 0.74 SP/SP 1500 1.6 1.5 0.79 SP/SP 1500 1.7 1.6 0.85 SP/SP 1900 1.7 1.6 0.85 SP/SP 1200 1.8 1.7 0.90 DF/DF 2100 1.8 1.7 0.90 DF/DF 2100 1.8 1.7 0.90 SP/SP 2100 1.8 0.7 0.90 SP/SP 2100 1.9 1.8 0.95 SP/SP 2400 2.0 1.9 1.8 0.95 SP/SP 2400 2.0 1.9 1.00	DF/DF 1600 1.6 1.5 0.79 560 DF/DF 1600 1.6 1.5 0.79 560 HF/HF 1350 1.5 1.4 0.74 375 DF/DF 1600 1.7 1.6 0.85 560 DF/DF 1600 1.7 1.6 0.85 560 HF/HF 1350 1.5 1.4 0.74 375 SF/SP 1450 1.6 1.5 0.79 650 SF/SP 1450 1.6 1.5 0.79 650 SF/SP 1550 1.5 1.4 0.74 650 SF/SP 1550 1.6 1.5 0.79 650 SF/SP 1550 1.6 1.5 0.79 650 SF/SP 1600 1.7 1.6 0.85 650 DF/DF 1900 1.7 1.6 0.85 650 DF/DF 1900 1.7 1.6 0.85 560 SF/SP 1500 1.6 1.5 0.79 650 SF/SP 1900 1.7 1.6 0.85 375 HF/HF 1900 1.7 1.6 0.85 375 HF/HF 1900 1.7 1.6 0.85 375 HF/HF 1900 1.7 1.6 0.85 375 DF/DF 2100 1.8 1.7 0.90 560 DF/DF 2100 1.8 0.7 0.90 560 DF

a) Design values are applicable to beams that have up to 2/3 of the depth on the compression side removed by taper cutting.

b) Tabulated design values apply only to tapered portion of member.

c) Shear design value has been reduced for non-prismatic members.

ANNEX B LAY-UP REQUIREMENTS FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER

TABLE	R1
17 (DEL	ים

LAY-UP REQUIREMENTS FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER COMBINATIONS

VISUC	y Gro	ided Wester										
T &		4–10 Lams			11 or More La	ms						
3 D	5%	L3 DF	_	10%	L3 DF	_						
16F-V3 DF (Unbalanced)	_	L3 DF	_	_	L3 DF	_						
on P	 5%	_	_	5% 5%	L2 DF	_						
	Э%	L2 DF			L1 DF	_						
50	5 01	4–10 Lams		_	11 or More La	ms						
nce /or	5% —	L2 DF	_	5% 5%	L1 DF L2 DF	_						
(Balanced)	_	L3 DF	_	_	L3 DF	_						
<u>e</u>	 5%	L2 DF	_	5% 5%	L2 DF L1 DF	_						
-		4–10 Lams			⊥ 11 or More La	ıms						
្ន ខ្ល	10%	L2 DF		5%	L2 DF	_	_					
2 =	-	_	_	-	_	_						
20F-V3 DF (Unbalanced)	_	L3 DF	_	5%	L3 DF L2 DF	_ 						
.5	5%	302-20 DF	_	5%	302-20 DF	_						
T =		4–10 Lams										
ZOF-V3 DF (Alternate)	20%	L2 DF	_									
ZUF-V3 DF (Alternate)	_	L3 DF	_									
₽ Z	20% 15%	L2 DF L1 DF	_ _ _ _									
	13%				11 or More La	una c	1					
٦ <u>و</u>	5%	4-10 Lams 302-20 DF		5%	302-20 DF	1115						
(Balanced)	5% 5%	L2D DF	_	5% 5%	L2 DF	_						
Balc Balc	_	L3 DF	_	 5%	L3 DF L2 DF	_						
7	5%	302-20 DF	_	5%	302-20 DF	_						
		4–10 Lams			8–10 Lams							
20F-V7 DF (Alternate)	10%	L1 DF	_	15%	L1 DF	_						
20F-V7 DF (Alternate)	_	 L3 DF	_	_	 L3 DF	_						
A	_	_	_	_	_	_						
	10%	L1 DF	_	15%	L1 DF	_						
O D		4–7 Lams			8–10 Lams			11–18 Lams			19 or More La	ms
20F-V12 AC (Unbalanced)	10% 15%	L1D AC L2 AC	_	10% 15%	L1D AC L2 AC	_	10% 15%	L1D AC L2 AC	_	10% 15%	L1D AC L2 AC	_
- 9 9	—	L3 AC	_	_	L3 AC	_	_	L3 AC	_	_	L3 AC	_
20F Unk	10% 25%	L2 AC L1D AC	_	10% 30%	L2 AC L1D AC	_	10% 10%	L2 AC L1S AC	_	10% 10%	L2 AC L1S AC	_
	5%	302-20 AC	1:14	5%	302-20 AC	1:14	5%	302-24 AC	_	5%	302-26 AC	_
		4–7 Lams			8–10 Lams			11 or More La	ms			
A G	5%	302-20 AC	1:16	5%	302-22 AC	_	5%	302-24 AC	_			
/13 ince	10% 10%	L1S AC L1D AC	_	10% 10%	L1S AC L1D AC	_	5% 10%	L1S AC L1D AC	_			
20F-V13 AC (Balanced)	—	L3 AC	_	_	L3 AC	_	_	L3 AC	_			
(E 2	10% 10%	L1D AC L1S AC	_	10% 10%	L1D AC L1S AC	_	10% 5%	L1D AC L1S AC	_			
	5%	302-20 AC	1:16	5%	302-22 AC		5%	302-24 AC	_			
O ē		4–7 Lams			8–10 Lams			11 Lams			12 or More La	ms
a PC	5%	L1D POC	_	5% 5%	L1D POC L2 POC	_	5% 5%	L1D POC L2 POC	_	10% 5%	L1D POC L2 POC	_
20F-V14 POC (Unbalanced)	_	L3 POC	_	- -	L2 POC	_	_	L2 POC	_	_	L3 POC	_
유	— 10%	L2 POC	_	— 10%	— L1D AC	_	 10%	L1D POC	_	5% 5%	L2 POC L1D POC	_
27	5%	302-20 POC	1:14	5%	302-20 AC	1:14	5%	302-24 POC	_	5% 5%	302-24 POC	
		4–7 Lams			8–10 Lams			11 Lams			12 or More La	ms
		302-20 POC	1:14	5%	302-20 POC	1:14	5%	302-24 POC	_	5%	302-24 POC	_
о (р	5%	L2 POC	_	10%	L1D POC	_	10%	L1D POC	_	5% 5%	L1D POC L2 POC	_
I5 POC nced)	5% 10%	L2 POC				_	_	_	_	370	12.00	
:-V15 POC alanced)		L2 POC — L3 POC	_	_	L3 POC	_	_	L3 POC	_		L3 POC	_
20F-V15 POC (Balanced)		_	_ _ _ _	 10%	L3 POC — L1D POC	_	_ _ 10%	L3 POC — L1D POC	_	5% 5%	L3 POC L2 POC L1D POC	=

		4–7 Lams			8–10 Lams			11 or More La	ms
(Unbalanced)	10% 10% — 15% 10% 5%	L2D DF L2 DF L3 DF L2 DF L1 DF 302-20 DF	_ _ _ _ _ 1:14	10% 10% — 15% 10% 5%	L2D DF L2 DF L3 DF L2 DF L1 DF 302-22 DF	_ _ _ _ _	10% 10% — 10% 5% 5%	L2D DF L2 DF L3 DF L2 DF L1 DF 302-24 DF	_ _ _ _ _
± ⊕	000/	4–7 Lams		000/	8–10 Lams			11 or More La	ms
24F-V5 DF/HF (Unbalanced)	20% 20% — 20% 15% 5%	L2D DF L2 HF L3 HF L1 HF L1 DF 302-20 DF	 1:14	20% 20% — 20% 15% 5%	L2D DF L2 HF L3 HF L1 HF L1 DF 302-22 DF	_ _ _ _ _	10% 10% — 20% 10% 5%	L2D DF L2 HF L3 HF L1 HF L1 DF 302-24 DF	_ _ _ _ _
		4–7 Lams			8–10 Lams			11 or More La	ms
24F-V8 DF (Balanced)	5% 5% 10% — 10% 5% 5%	302-20 DF L1 DF L2 DF L3 DF L2 DF L1 DF 302-20 DF	1:14 — — — — — — 1:14	5% 5% 10% — 10% 5% 5%	302-22 DF L1 DF L2D DF L3 DF L2D DF L1 DF 302-22 DF	_ _ _ _ _ _	5% 5% 5% — 5% 5% 5%	302-24 DF L1 DF L2 DF L3 DF L2 DF L1 DF 302-24 DF	_ _ _ _ _ _
		4–7 Lams			8–10 Lams			11 or More La	ms
24F-V10 DF/HF (Balanced)	5% 15% 10% — 10% 15% 5%	302-20 DF L1 DF L2 HF L3 HF L2 HF L1 DF 302-20 DF	1:14 — — — — — 1:14	5% 15% 10% — 10% 15% 5%	302-22 DF L1 DF L2 HF L3 HF L2 HF L1 DF 302-22 DF	 	5% 10% 15% — 15% 10% 5%	302-24 DF L1 DF L2 HF L3 HF L2 HF L1 DF 302-24 DF	- - - - -
()		4–7 Lams			8–10 Lams			11 or More La	ms
26F-V1 DF (Unbalanced)	25% 5% — 5% 20% 5%	L1 DF L2D DF L3 DF L2D DF L1 DF 302-22 DF	_ _ _ _ _	25% 5% — 5% 20% 5%	L1 DF L2D DF L3 DF L2D DF L1 DF 302-24 DF	_ _ _ _ _ _	25% 5% — 5% 20% 5%	L1 DF L2D DF L3 DF L2D DF L1 DF 302-26 DF	_ _ _ _ _ _
		4–7 Lams			8–10 Lams			11 or More La	ms
26F-V2 DF (Balanced)	5% 20% 5% — 5% 20% 5%	302-22 DF L1 DF L2D DF L3 DF L2D DF L1 DF 302-22 DF	— — — — —	5% 20% 5% — 5% 20% 5%	302-24 DF L1 DF L2D DF L3 DF L2D DF L1 DF 302-24 DF	— — — — —	5% 20% 5% — 5% 20% 5%	302-26 DF L1 DF L2D DF L3 DF L2D DF L1 DF 302-26 DF	
E-Rate	ed We	stern Specie							
HE ced)	10%	4-10 Lams 1.6E2 HF		5%	1.6E2 HF	ms 	_		
16F-E2 HF (Unbalanced)	— — — — 5%	L3 HF — 302-20 HF	 1.6E4	5% 5% 5%	L3 HF 1.6E2 HF 302-20 HF	— — — 1.6E4			
L _		4–7 Lams			8–10 Lams				
16F-E2 HF (Alternate)	10% — —	1.9E2 HF — L3 HF	_ _ _	20% — —	1.6E2 HF — L3 HF	_ _ _			
25	10%	1.9E6 HF	_	30%	1.6E4 HF	_			
L p		4–7 Lams		1	11 or More La	ms			
3 D	10%	1.9E2 DF	_	5%	1.9E2 DF —	_			
16F-E3 DF (Unbalanced)	 10%	L3 DF — 1.9E6 DF	_ _ _ _	 _ _ 5%	L3 DF — 302-20 DF	— — — 1.9E6	-		
₽ (p	100/	4–10 Lams			11 or More La				
16F-E6 DF (Balanced)	10% — — —	1.9E6 DF — L3 DF —	_ _ _ _	5% — —	302-20 DF — L3 DF —	1.9E6 — — —			

		QUIREMEN 4 or More Lai		кэн	COCTORA	LGLUE	D LA	MINAIED	JOFIN	VOO	DIIMBEK	COMB	IIVAI	10143	
16F-E7 HF (Balanced)	5%	302-20 HF	1.6E4												
alan alan	5% —	1.6E4 HF L3 HF	_												
9 8	5% 5%	1.6E4 HF 302-20 HF	 1.6E4												
ш		4–7 Lams			8–10 Lams	;									
16F-E7 HF (Alternate)	10%	1.9E6 HF	_	30%	1.6E4 HF	_									
Fer	_	L3 HF	_	_	L3 HF	_									
25	10%	— 1.9E6 HF	_	30%	— 1.6E4 HF	_									
<u>-</u>		4–7 Lams			8–10 Lams			11 or More Lo	ms						
20F-E2 HF (Unbalanced)	10%	1.9E2 HF	_	10%	1.9E2 HF	_	20%	1.9E2 HF	_						
7.		L3 HF	_		L3 HF	_	_	L3 HF	_						
20	15% 5%	1.6E4 HF 1.9E6 HF	_	10% 5%	1.6E4 HF 1.9E6 HF	_	15%	— 1.9E6 HF	_						
	5%	302-20 HF	1.9E6	5%	302-20 HF	1.9E6	5%	302-20 HF	1.9E6						
₽	10%	4–10 Lams 1.9E2 HF													
-E2	-	_	_												
20F-E2 HF (Alternate)	10% 10%	L3 HF 1.9E6 HF 2.1E6 HF	_ _ _												
⊥ (pe		4–10 Lams			11–13 Lam	S		14 or More Lo	ms	_					
E3 D	10%	1.9E2 DF —	_	15%	1.9E2 DF —	_	15%	1.9E2 DF —	_						
20F-E3 DF (Unbalanced)	 15% 5%	L3 DF 1.9E6 DF 302-20 DF	 1.9E6	 15% 5%	L3 DF 1.9E6 DF 302-22 DF	— — 1.9E6	 10% 5%	L3 DF 1.9E6 DF 302-22 DF	— — 1.9E6						
		4–10 Lams							,	J					
20F-E3 DF (Alternate)	20%	2.1E2 DF	_												
Ferr F	10%	1.9E2 DF L3 DF	_												
≥2	10% 20%	1.9E6 DF 2.1E6 DF	_												
ш.		4–10 Lams			11–13 Lam	s		14 or More Lo	ıms]					
20F-E6 DF (Balanced)	5%	302-20DF	1.9E6	5%	302-22DF	1.9E6	5% 10%	302-22DF	1.9E6						
Salar Salar	15%	1.9E6 DF L3 DF	_	15%	1.9E6 DF L3 DF	_	l —	1.9E6 DF L3 DF	_						
2 = 3	15% 5%	1.9E6 302-20 DF	 1.9E6	15% 5%	1.9E6 302-22 DF	— 1.9E6	10% 5%	1.9E6 DF 302-22 DF	— 1.9E6						
L _		4–10 Lams								•					
20F-E6 DF (Alternate)	20% 10%	2.1E6 DF 1.9E6 DF	_												
PF-F	_	L3 DF	_												
<u>~</u>	10% 20%	1.9E6 DF 2.1E6 DF	_												
		4–7 Lams			8–10 Lams			11 or More Lo	ms						
₩ (p	5% 5%	302-20 HF 1.9E6 HF	1.9E6	5% 5%	302-22 HF 1.9E6 HF	1.9E6 —	5% 15%	302-22 HF 1.9E6 HF	1.9E6 —						
-E7	15%	1.6E4 HF	=	10%	1.6E4 HF	_	_	_	_						
20F-E7 HF (Balanced)	15%	L3 HF 1.6E4 HF	_	10%	L3 HF 1.6E4 HF	_	_ _	L3 HF —	_ _ _						
	5% 5%	1.9E6 HF 302-20 HF	 1.9E6	5% 5%	1.9E6 HF 302-22 HF	— 1.9E6	15% 5%	1.9E6 HF 302-22 HF	— 1.9E6						
		4–10 Lams								J					
7 H	10% 10%	2.1E6 HF	_												
20F-E7 HF (Alternate)	 10%	1.9E6 HF L3 HF 1.9E6 HF	_												
	10%	2.1E6 HF 4-7 Lams			8–9 Lams			9–13 lams			14–16 Lam			17 or More Lo	ıms
20F-E8 ES (Unbalanced)	10%	C6 ES	_	10%	C6 ES	_	15%	C6 ES	_	10%	C6 ES	_	15%	C6 ES	_
lanc	15%	D4 ES D ES	_	15%	D4 ES D ES	_	10%	D4 ES D ES	_	15%	D4 ES D ES	_	10%	D4 ES D ES	=
20F. Jnba	15%	C4 ES	_	15%	C4 ES	=	10%	C4 ES	=	10%	C4 ES B ES	_	10% 10%	C4 ES B ES	_
5	5% 5%	B ES 302-20 ES	B ES	5% 5%	B ES 302-22 ES	B ES	15% 5%	B ES 302-22 ES	B ES	10% 5%	302-24 ES	B ES	5%	302-24 ES	B E

											D TIMBER				
E 📻	5%	4-7 Lams 302-24 SPF	2.0E6	5%	8 or More La 302-24 SPF	ms 2.0E6									
24F-E/SPF1 (Balanced)	15% 5% —	2.0E6 SPF 1.8E3 SPF 1.4E2 SPF	_ _ _	10%	1.8E3 SPF — 1.4E2 SPF	_ _ _									
24F (Bc	5% 15% 5%	1.8E3 SPF 2.0E6 SPF 302-24 SPF	 2.0E6	10% 5%	 1.8E3 SPF 302-24 SPF	 2.0E6									
	370	4–7 Lams	2.020		8 or More La										
P.T.3	20%	L2D DF	_	5%	L2D DF	_									
24F-E/SPF3 (Unbalanced)	5% — 5%	1.8E3 SPF 1.4E2 SPF 1.8E3 SPF	_ _ _	10%	1.8E3 SPF 1.4E2 SPF —	_ _ _									
4⊃	15% 5%	2.0E6 SPF 302-24 SPF	 2.0E6	10% 5%	1.8E3 SPF 302-24 SPF	 2.0E6									
		4–10 Lams			11–13 Lam	S		14-15 Lam	s	1	l 6 or More La	ıms]		
24F-E4 DF (Unbalanced)	20% 20%	2.1E2 DF 1.9E2 DF L3 DF	_ _	10% 20%	2.1E2 DF 1.9E2 DF L3 DF	_ _ _	10% 15%	2.1E2 DF 1.9E2 DF L3 DF	_ _ _	10% 10%	2.1E2 DF 1.9E2 DF L3 DF	_			
24F (Unbo	20% 15% 5%	1.9E6 DF 2.1E6 DF 302-20 DF	 2.1E6	30% 5% 5%	1.9E6 DF 2.1E6 DF 302-22 DF	 2.1E6	15% 5% 5%	1.9E6 DF 2.1E6 DF 302-22 DF	— — 2.1E6	10% 5% 5%	1.9E6 DF 2.1E6 DF 302-24 DF	— — 2.1E6			
		4–8 Lams			9–13 Lams			14 or More Lo				20	J		
24F-E11 HF (Unbalanced)	5% 5%	302-20 HF 2.1E6 HF	2.1E6 —	5% 5%	302-22 HF 2.1E6 HF	2.1E6 —	5% 5%	302-24 HF 2.1E6 HF	2.1E6 —						
F.E.	10%	1.9E6 HF L3 HF	_	10%	1.9E6 HF L3 HF	_	10%	1.9E6 HF L3 HF	_						
2 2⊓	10% 5%	1.9E6 HF 2.1E6HF	_	10% 5%	1.9E6 HF 2.1E6HF	_	10% 5%	1.9E6 HF 2.1E6HF	_						
	5%	302-20 HF	2.1E6	5%	302-22 HF	2.1E6	5%	302-24 HF	2.1E6				1		
ш	5%	4-10 Lams 302-22 DF	2.1E6	5%	11–13 Lams 302-24 DF	2.1E6	5%	14-15 Lam 302-24 DF	2.1E6	5%	302-24 DF		-		
24F-E13 DF (Balanced)	15% 20%	2.1E6 DF 1.9E6 DF L3 DF		5% 30%	2.1E6 DF 1.9E6 DF L3 DF	2.1E6 —	5% 15%	2.1E6 DF 1.9E6 DF L3 DF	2.1E0 — —	5% 10%	2.1E6 DF 1.9E6 DF L3 DF	2.1E6 — —			
24F (Bc	20% 15% 5%	1.9E6 DF 2.1E6 DF 302-22 DF	 2.1E6	30% 5% 5%	1.9E6 DF 2.1E6 DF 302-24 DF	 2.1E6	15% 5% 5%	1.9E6 DF 2.1E6 DF 302-24 DF	— — 2.1E6	10% 5% 5%	1.9E6 DF 2.1E6 DF 302-24 DF	 2.1E6			
	0,0	4–7 Lams	220	0,0	8–10 Lams		0,0	11–14 Lam:		070	15–19 Lam:		2	20 or More Lo	ıms
15 HF	10% 10%	2.1E2 HF 1.6E4 HF	_	10% 15%	2.1E2 HF 1.6E4 HF	_	10% 10%	1.9E2 HF 1.6E4 HF	_	10% 10%	2.1E2 HF 1.6E4 HF	_	10% 15%	2.1E2 HF 1.6E4 HF	=
24F-E15 HF (Unbalanced)	10% 5%	L3 HF 1.6E4 HF 2.1E6 HF	_ _ _	10% 5%	L3 HF 1.9E2 HF 2.1E6 HF	_ _ _	10% 5%	L3 HF 1.9E2 HF 2.1E3 HF	_ _ _	 10% 5%	L3 HF 1.9E2 HF 2.1E3 HF	_ _ _	— 10% 5%	L3 HF 1.9E2 HF 2.1E3 HF	_ _
	5%	302-20 HF	2.1E6	5%	302-20 HF	2.1E6	5%	302-24 HF	2.1E3	5%	302-24 HF	2.1E3	5%	302-24 HF	2.1E
ш	5%	4-8 Lams 302-20 DF	2.2E6	5%	9–11 Lams 302-22 DF	2.2E6	5%	12-15 Lam	2.2E2	5%	302-22 DF	2.2E2	_		
F-E18 DF alanced)	5% —	2.2E6 DF — L3 DF		5% 10%	2.2E6 DF 1.9E6 DF L3 DF		5% 5%	2.2E2 DF 1.9E2 DF L3 DF		5% 10%	2.2E2 DF 1.9E2 DF L3 DF				
24F - (Bal	5% 5%	— 2.2E6 DF 302-20 DF	 2.2E6	10% 5% 5%	1.9E6 DF 2.2E6 DF 302-22 DF	 2.2E6	5% 5% 5%	1.9E2 DF 2.2E2 DF 302-22 DF	 2.2E2	10% 5% 5%	1.9E2 DF 2.2E2 DF 302-22 DF	 2.2E2			
√isua	lly Gro	aded Southe	ern Pine												
6		4 or More La	ms												
V2 S	10%	N2M	_												
16F-V2 SP (Unbalanced)	_	N2M	_												
_5	5%	NID	_												
G (0)		4–8 Lams			9–10 Lams										
V2 S	10%	N2M —	_	10%	N2M —	_									
16F-V2 SP (Alternate)	10% 10%	N3M N2M N1D	1:8 — 1:12	10% 10%	N3M N2M N2D	1:8 — 1:12									
<u>_</u>		4–10 Lams			11 or More Lo										
73 SI	10%	N2D	_	5%	N2D	_									
16F-V3 SP (Unbalanced)	 5%	— N3M N2D	1.8	_ _	N3M —	1.8									

0	PKEG	SOIKEWEL	NTS FO	R STI	RUCTURAI	. GLUE	D LA	MINATED	SOFT	VOOL	TIM
.		4–8 Lams			9–10 Lams						
16F-V3 SP (Alternate)	10%	N2D	_	10%	N2D	_					
\ ter		N2M	_		N2M	_					
	25% 5%	N2D N2D	— 1:10	5% 5%	N2D N2D	1:10					
		4 or More La	ms				J				
5 S	5%	N1M	_								
16F-V5 SP (Balanced)	5% —	N2M N2M	1:10 —								
9 (B)	5% 5%	N2M N1M	1:10								
		4–8 Lams			9–10 Lams						
16F-V5 SP (Alternate)	5%	N2D	1:10	5%	N2D	1:10					
F- K	25%	N2D N2M	_	5%	N2D N2M	_					
<u>9</u> ₹	25%	N2D	_	5%	N2D	_					
	5%	N2D 4–10 Lams	1:10	5%	N2D I 1 or More La	1:10 ms					
20F-V2 SP (Unbalanced)	10%	N2D	_	15%	N2D	_					
-V2 Ilan		 N3M	— 1:8	_	 N3M	 1:8					
20 F. Inba	10%	N2M	_	5%	N2M	1:10					
.,5	5% 5%	N1D 302-20	1:12 —	 5%	— 302-20	_					
۵		4–8 Lams			9–10 Lams						
20F-V2 SP (Alternate)	10%	N1D	_	10%	N1M	1:14					
Fr.	10%	N2M N3M	— 1:8	15% —	N2M N3M	1:8					
≥%	10% 20%	N2M N1D	_	10% 20%	N2M N1D	1:12					
=	2070	4–10 Lams		2070	11–12 Lams		1	3 or More Lo	ams		
20F-V3 SP (Unbalanced)	5%	N2M	_	5%	N2M	_	5%	N2M	_		
		N2M	_	_	— N2M	_	_	N2M	_		
20	5% 5%	N1D 302-20	_	 5%	302-20	_	5% 5%	N2M 302-20	1:10		
	3%	4-8 Lams	_	3%	9–10 Lams		3%	302-20	_		
20F-V3 SP (Alternate)	10%	N2D	_	10%	N2D	_					
ernc	_	N2M	_	_	N2M	_					
<u>₹</u>		_	_	15%	N1D						
	25%	N1D	_	5%	N1D	1:12	,	1 or More Lo			
۵.	5%	4-8 Lams 302-20	_	5%	9-10 Lams 302-20	_	5%	302-20	anis		
F-V5 SP Ilanced)	5%	N1D	_	_	_	_	5%	N2D	1:12		
alan	10%	N2M N3M	— 1:8	15% —	N2D N3M	1:8	5% —	N2D N3M	1.8		
90 (Ba	10% 5%	N2M N1D	_	15%	N2D —	_	5% 5%	N2D N2D	 1:12		
	5%	302-20	_	5%	302-20	_	5%	302-20			
e) SP		4–8 Lams			9–10 Lams						
20F-V5 SP (Alternate)	10% 10%	N1D N2D	_	10% 10%	N1D N2D	1:12					
Alte	10%	N3M N2D	1:8	10%	N3M N2D	1:8					
(4 ·	10%	N1D	_	10%	N1D	1:12					
		4–8 Lams			9–10 Lams		1	1 or More Lo	ams		
24F-V1 SP (Unbalanced)	10%	N1D —	_ _ _	5% 10%	N1M N1M	1:12	15%	N1M	1:12		
alg	10%	N2D		15%	N2M	_ _	15%	N2M	_ _ 1.0		
24 F Unb.	15%	N3M N2D	1:8 — —	15%	N3M N2M	1:8	 15%	N3M N2M	1:8		
=	5% 5%	N1D 302-20	— 1:14	10% 5%	N1D 302-22	_	10% 5%	N1D 302-24	1:12		
	570	4-8 Lams	7.1.4	370	9–10 Lams			1 or More Lo	ams		
sp nced)	10%	N1D	_	10%	NID	_	10%	N1D	_		
24F-V3 SP (Unbalanced)	10%	N2D N2M	_ _ _	10%	N2D N2M	_	10%	N2D N2M	_ _ _		
24F Unb	15% 5%	N2D N1D	_	15% 5%	N2D N1D	 1:12	15% 5%	N2D N1D	— 1:12		
_	5%	302-20	1:14	5%	302-22	1.12	5%	302-24	1.12		

TABLE B1 (Continued)

LAY-UP REQUIREMENTS FOR STRUCTURAL GLUED LAMINATED SOFTWOOD TIMBER COMBINATIONS

11 or More Lams

N1M N1M

N1M N2M N3C N2M N1D

302-24

5% 10%

10%

20% 10% 5% 1:14 1:12

1:8

1:14

S	.A1-UI	P KEC		NIS FO	K 511	RUCTURA	LGLUE	D LA		
10% N1M			4–5 Lams			6–8 Lams			9–10 Lams	
15% NID	.V4 SP lanced)	10%	N1M N2M	_	5%	N1M N2M	_	5%	N1M N1M N2M	1:12 — —
S	24F - (Unba	25%	N3C N2M N1D	_	15%	N3C N2M N1D	_	15%	N3C N2M N1D 302-22	1:8 — — —
S			4–8 Lams			9–10 Lams			11 or More Lo	ıms
	24F-V5 SP (Balanced)	5% 10% — 10% 5%	N1D N2D N2M N2D N1D	_ _ _ _ _	5% 5% — 5% 5%	N1D N2D N2M N2D N1D	_ _ _ _ _	5% 5% — 5% 5%	302-24 N1D N2D N2M N2D N1D 302-24	1:12 1:10 — 1:10 1:12
S									11 or More Lo	ıms
T-8 Lams 9-10 Lams 11 or Mo	24F-V8 SP (Balanced)	5% 10% — 10% 5%	302-20 N1D N2D N2M N2D N1D	_ _ _ _	5% 5% — 5% 5%	302-22 N1D N2D N2M N2D N1D	_ _ _ _ _	5% 5% 10% — 10% 5%	302-24 N1D N2D N2M N2D N1D 302-24	1:12 1:10 — 1:10 1:12
10 10 10 10 10 10 10 10			7–8 Lams			9–10 Lams			11 or More Lo	ıms
10 10 10 10 10 10 10 10	V1 SP lanced)	20% —	NID —	_			1:12 —	5%	N1D N1D N2D	1:12 —
T-8 Lams 9-10 Lams 11 or Mo	26F -		— N1D	_ _ _		— N1D	_ _ _	15% 5%	N2M N2D N1D 302-26	1:10 1:14
20% NID 5% NID 1:12 1:12 5% NID 1:12 1:12 1:12 1:12 1:12 1:12 1:12 1:12 1:12 1:		370			370				11 or More Lo	ıms
S	26F-V2 SP Inbalanced)	_	N1D — N2D —	_ _ _	15% —	N1D N1D N2D —		5% 20% — 15%	N1D N1D N2D N1D	1:12 — — —
20% NID	⊆			_		N1D 302-24	_		N1D 302-26	1:12 —
5% 302-22 — 5% 302-24 — 5% 302-2 7-8 Lams 9-10 Lams 11 or Mo			7–8 Lams			9–10 Lams			11 or More Lo	ıms
5% 302-22 — 5% 302-24 — 5% 302-2 7-8 Lams 9-10 Lams 11 or Mo	4F-V3 SP	_	_	_ _ _ _	15% —	N1D N1D N1M —	1:12 — — —	20%	NID NID NIM NID	1:12 — — — — 1:12
7-8 Lams 9-10 Lams 11 or Mo	~⊃			_			_	5% 5%	N1D 302-26	1:12
5% 302-22 — 5% 302-24 — 5% 302-2 5% NID 1:12 5% NID 1:12 5% NID 1:12 5% NID 1:12 5% NID 1:15% N									11 or More Lo	ıms
15% NID — 15% NID — 15% NID 1:12 5% NID	26F-V4 SP (Balanced)	5% 15% — 15% 5%	N1D N1D N1M N1D N1D	_ _ _	5% 15% — 15% 5%	N1D N1D N1M N1D N1D	_ _ _	5% 15% — 15% 5%	302-26 N1D N1D N1M N1D N1D 302-26	1:12 1:12
7–8 Lams 9–10 Lams 11 or Mo			7–8 Lams			9–10 Lams			11 or More Lo	ıms
S	26F-V5 SP (Balanced)	5% 15% — 15% 5%	N1D N1D N2D N1D N1D	_ _	5% 15% — 15% 5%	N1D N1D N2D N1D N1D	_	5% 15% — 15% 5%	302-26 N1D N1D N2D N1D N1D N1D 302-26	1:12 — — — — 1:12

-Rate		thern Pine								1001	TIMBER	COMB	
		4 or More La	ms										
E1 SP lancec	5% —	1.9E2 —	_										
16F-E1 SP (Unbalanced)	5% 5%	N2M 1.9E6 302-20	— — 1.9E6										
	0,0	4–10 Lams											
16F-E1 SP (Alternate)	10%	1.9E2	_										
F.F	_	N2M	_										
<u>9</u> ₹	 10%	_	_										
		2.1E6 4 or More La	me										
16F-E3 SP (Balanced)	10%	1.9E6	_										
E 20	_	_	_										
Ba	_	N2M —	_										
	10%	1.9E6	_							_			
a (p)	100/	4-8 Lams		100/	9–10 Lams		E0/	11–13 Lam			4 or More L		
20F-E1 SP (Unbalanced)	10%	1.9E2 —	_	10% —	1.9E2 —	_	5% —	1.9E2 —	_	15% —	1.9E2 —	_	
lpd lpd		N2M 	_	— 10%	N2M 1.9E6	_	— 5%	N2M 1.9E6	_		N2M	_	
Ž,	5% 5%	2.1E6 302-20	 2.1E6	5% 5%	2.1E6 302-20	 2.1E6	 5%	 302-20	 2.1E6	10% 5%	1.9E6 302-20	 1.9E6	
	370	4-8 Lams	2.110	370	9–10 Lams		370	302-20	2.160	3%	302-20	1.960	
20F-E1 SP (Alternate)	10%	2.1E2	_	10%	2.1E2	_							
ern.	_	 N2M	_	_	 N2M	_							
2 ₹	_	_	_	15%	1.9E6	_							
	25%	2.1E6	_	15%	2.1E6	_							
g (p	5%	4-10 Lams 302-20	1.9E6	5%	302-20	2.1E6	5%	302-20	1.9E6				
.E3	15%	1.9E6	-	5%	1.9E6		10%	1.9E6	-				
20F-E3 SP (Balanced)	— 15%	N2M 1.9E6	_	— 5%	N2M 1.9E6	_	— 10%	N2M 1.9E6					
	5%	302-20	1.9E6	5%	302-20	2.1E6	5%	302-20	1.9E6				
e SP	0.50/	4–8 Lams		100/	9–10 Lams								
20F-E3 SP (Alternate)	25% 10%	2.1E6 1.9E6	_	10% 10%	2.1E6 1.9E6	_							
20F-E3 (Alterna	10%	N2M 1.9E6	_ _	— 10%	N2M 1.9E6	_							
	25%	2.1E6		10%	2.1E6								
- - - -		4–8 Lams			9–10 Lams		1	11 or More Lo	ıms				
E1 SP lanced)	10%	2.1E2	_	10%	2.1E2	_	20%	1.9E2 —	_				
iF-E bala	_	N2M	_	_	N2M	_	_	N2M	_				
24F-1 (Unbal	25% 5%	1.9E6 2.1E6	_	20% 5%	1.9E6 2.1E6	_	10% 5%	1.9E6 2.1E6	_				
	5%	302-20	2.1E6	5%	302-22	2.1E6	5%	302-24	2.1E6				
	E0/	4-8 Lams	0.157	F0/	9–10 Lams			11 or More Lo					
24F-E4 SP (Balanced)	5% 15%	302-20 2.1E6	2.1E6 —	5% 15%	302-22 2.1E6	2.1E6 —	5% 15%	302-24 2.1E6	2.1E6 —				
H G	10%	1.9E6 N2M	_	10%	1.9E6 N2M	_	10%	1.9E6 N2M	_				
(Bc	10%	1.9E6	_	10%	1.9E6	_	10%	1.9E6	_				
	15% 5%	2.1E6 302-20	2.1E6	15% 5%	2.1E6 302-22	 2.1E6	15% 5%	2.1E6 302-24	 2.1E6				
		4–10 Lams		1	1 or More Lo	ıms							
(Unbalanced)	10%	N1D 2.3E	1:12	10%	N1D 2.3E	1:12							
alar alar	10%	N1D 2.0E N2M	_	15% —	N1D 2.0E N2M	_							
28 Unb	10% 15%	N1D 2.0E N1D 2.3E	_	15% 5%	N1D 2.0E N1D 2.3E	_							
	5%	302-28	2.3E5	5%	302-30	2.3E5							

		4–10 Lams		1	11 or More La	ıms
28F-E2 SP (Balanced)	5% 15% 10% — 10% 15% 5%	302-28 N1D 2.3E N1D 2.0E N2M N1D 2.0E N1D 2.3E 302-28	2.3E5 — — — — — — 2.3E5	5% 5% 15% — 15% 5% 5%	302-30 N1D 2.3E N1D 2.0E N2M N1D 2.0E N1D 2.3E 302-30	2.3E5 — — — — — — 2.3E5
_		4–10 Lams		1	I1 or More La	ıms
30F-E1 SP (Unbalanced	10% 20%	N1D 2.3E N1D 2.0E N2M	_ _ _	15% 15% —	N1D 2.3E N1D 2.0E N2M	_
30F (Unb	10% 15% 5%	N1D 2.0E N1D 2.3E 302-28	 2.3E5	15% 5% 5%	N1D 2.0E N1D 2.3E 302-30	 2.3E5
		4–10 Lams		1	11 or More La	ms
30F-E2 SP (Balanced)	5% 15% 10% — 10% 15% 5%	302-28 N1D 2.3E N1D 2.0E N2M N1D 2.0E N1D 2.3E 302-28	2.3E5 — — — — — — 2.3E5	5% 5% 15% — 15% 5% 5%	302-30 N1D 2.3E N1D 2.0E N2M N1D 2.0E N1D 2.3E 302-30	2.3E5 — — — — — — — 2.3E5
Califo	rnia R	edwood				
		4–7 Lams			8–10 Lams	

*30F combinations are restricted to a maximum 6 in. nominal width unless the manufacturer has qualified for wider widths based on full-scale tests subject to approval by an accredited agency.

Califo	ornia R	ledwood							
		4–7 Lams		8–10 Lams	;		11 or More Lo	ıms	
2	5%	302-20	L1 or L2	5%	302-22	L1 or L2	5%	302-24	L1 or L2
5 6	25%	L1 or L2	_	20%	L1 or L2	_	20%	L1 or L2	_
 5 ≧	l —	_	_	5%	L3	_	5%	L3	_
alan	l —	L4 or L5	_	_	L4 or L5	_	_	L4 or L5	_
9 <u>9</u>	l —	_	_	5%	L3	_	5%	L3	_
	25%	L1 or L2	_	20%	L1 or L2	_	20%	L1 or L2	_
	5%	302-20	L1 or L2	5%	302-22	L1 or L2	5%	302-24	L1 or L2

Combination Symbol	Grade/ Species	Combination Symbol	Grade/ Species				
Douglas-	Fir-Larch	Southern Pine					
1	L3 DF	47	N2M12 SP				
2	L2 DF	47 1:10	N2M10 SP				
3	L2D DF	47 1:8	N2M SP				
4	L1CL DF	48	N2D12 SP				
5	L1 DF	48 1:10	N2D10 SP				
Hem	-Fir	48 1:8	N2DSP				
14	L3 HF	49	N1M16SP				
15	L2 HF	49 1:14	N1M14 SP				
16	L1 HF	49 1:12	N1M12 SP				
17	L1D HF	40 1:10	N1M SP				
Softw	oods	50	N1D14 SP				
22	L3SW	50 1:12	N1D12 SP				
Alaska	Cedar	50 1:10	N1D SP				
69	L3AC						
70	L2AC						
71	L1DAC						
72	L1S AC						
Port Orfo	rd Cedar						
73	L3 POC						
74	L2 POC						

L1D POC

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ANNEX C LAMINATING LUMBER GRADING RULES FOR STRUCTURAL GLUED LAMINATED TIMBERS

1. INTRODUCTION

Lumber shall be either visually graded or mechanically graded as required for the laminating combinations. Structural laminating lumber shall be graded on the basis of the dressed size of the lumber. The knot sizes for structural laminating grades of western species are based on a fraction of the dressed width of the piece of lumber. The knot sizes for structural joist and plank grades and structural light framing grades of all species are tabulated on the basis of the nominal width. When lumber is graded before being ripped or resawn, it shall be graded on the basis of the ripped or resawn size. Otherwise it shall be graded after being ripped or resawn. Where the finished width of the laminated timber is less than 85% of the dressed width of the lumber used for the laminations, the lumber shall be graded on the basis of the next smaller nominal width.

2. DEFINITIONS/MEASUREMENT OF CHARACTERISTICS

2.1 Moisture Content

The weight of the water in wood expressed in percentage of the weight of the oven-dry wood.

2.2 Knots

A portion of a branch or limb that has become incorporated in a piece of lumber.

Knots are permitted to be sound, unsound, or not firmly fixed. A knot shall be measured by the area of the cross section it occupies. For all lumber, knots shall be limited in size and spaced as described for specific grades herein.

2.3 Edge Knot

A knot located at the edge of the face in a piece of lumber. A wide face knot overlapping part of the edge shall be considered an edge knot if it occupies more than 1/2 the thickness.

2.4 Knotholes

The hole left when a "loose" knot falls or is forced from the lumber.

2.5 Slope of Grain

The deviation of the line of fibers from a straight line parallel to the sides of the piece.

2.6 Splits

A separation of the wood through the piece to the opposite surface or to an adjoining surface due to the tearing apart of the wood cells.

2.7 Shakes

A lengthwise separation of the wood which occurs between or through the rings of annual growth.

2.8 Checks

A separation of the wood normally occurring across or through the rings of annual growth and usually as a result of seasoning.

2.9 Warp

Any deviation from a true or plane surface, including bow, crook and cup or any combination thereof.

2.9.1 Bow

A deviation flatwise from a straight line drawn from end to end of a piece.

2.9.2 Crook

A deviation edgewise from a straight line drawn from end to end of a piece.

2.9.3 Cup

A deviation in the face of a piece from a straight line drawn from edge to edge of a piece.

2.10 Torn Grain

A manufacturing imperfection in the surface of a piece where wood has been torn or broken out by surfacing.

2.11 Raised Grain

A condition of the surface of dressed lumber in which the hard latewood is raised above the surface of the softer earlywood, but not torn loose from it.

2.12 Wane

Bark or lack of wood from any cause except eased edges, on the edge or corner of a piece of lumber.

2.13 Decay

A disintegration of the wood substance due to action of wood-destroying fungi, and is also known as dote or rot.

2.13.1 White Speck

A form of decay identified by small white or brown pits or spots in wood caused by fungi. It develops in the living tree and does not develop further in wood in service.

2.13.2 Honeycomb

A form of decay similar to white speck but the pockets are larger.

2.14 Compression Wood

Abnormal wood formed on the underside of leaning and crooked coniferous trees. It is characterized, aside from its distinguishing color, by being hard and brittle. It is identified by its relatively wide, usually eccentric annual rings, relatively large amount of latewood (sometimes more than 50% of the width of the annual rings in which it occurs), and its lack of demarcation between earlywood and latewood in the same annual rings.

2.15 Springwood or Earlywood

The less dense, larger-celled part of the growth layer formed first during the annual growth cycle.

2.16 Summerwood or Latewood

The denser, smaller-celled, later-formed part of a growth ring.

2.17 Growth Rate

A characteristic used to estimate specific gravity from the number of growth rings per inch along with the amount of summerwood.

3. GENERAL REQUIREMENTS

3.1 Moisture Content

Moisture content shall not exceed 16%. Moisture content determinations shall be based on ASTM D4442 or D4444. In-line moisture meters used for lumber segregation shall be calibrated using one of these standards.

The range of average moisture contents of pieces of lumber to be assembled into a single timber shall not exceed 5 percentage points if the average moisture content of any piece exceeds 12%. The moisture content of a piece of lumber shall be the average moisture content throughout the cross section and along the length of the piece.

Exception: when it is known that the in-use equilibrium moisture content of the laminated timber will be 16% or more, the moisture content of laminations at the time of bonding shall not exceed 20%. All bonding procedures for lumber with moisture content above 16% shall be qualified according to the requirements of ANSI A190.1. These qualification tests shall be performed using lumber with the maximum moisture content to be qualified (not to exceed 20%).

3.2 Surfacing and Cleanliness

At the time of bonding, variations in thickness across the width of a lamination shall not exceed plus or minus 0.008 inch. The variation in thickness along the length of an individual piece of lumber or the lamination shall not exceed plus or minus 0.012 inch. The thickness variation shall occur randomly across the width and along the length such that the cumulative effect does not contribute to side-to-side depth variations greater than allowed in ANSI A190.1. All bonding surfaces including face, edge and end joints shall be smooth and, except for minor local variations, shall be free of raised grain, torn grain, skip, burns, glazing or other deviations from the plane of the surface that might interfere with the contact of sound wood fibers in the mating surfaces. All bonding surfaces shall be free from dust, foreign matter, and exudation which are detrimental to satisfactory bonding.

When lumber will not be resurfaced prior to laminating, the grading process must contain adequate checks to assure that pieces not conforming to the tolerances stated above are excluded.

When lumber will be resurfaced after grading, pieces which will not, after being surfaced, conform to the tolerances stated above shall be excluded.

3.3 Knots

Knots shall be permitted to be sound, unsound, or not firmly fixed.

3.3.1 In or Near End Joints

Knots or knotholes in plane scarf joints shall be limited to those permitted for the lumber grade. In no case shall they exceed 1/4 the nominal width of the piece in laminations occupying the outer 10% on each side of bending members and in any lamination of tension members.

Finger joints shall not contain knots.

In bending members, knots exceeding 3/8-inch diameter shall not be permitted within 2 knot diameters or 6 inches, whichever is less, of finger joints in the inner and outer tension zones (in no case less than 10% of the depth of bending members). Knots over 1/2-inch diameter shall not be permitted within one knot diameter of finger joints in the balance of the laminations.

In tension members, knots larger than 3/8 inch shall not be permitted within 2 knot diameters or 6 inches, whichever is less, of finger joints in any lamination.

In compression members, knots larger than 3/4 inch shall not be permitted within one knot diameter of finger joints. Measurement of knot diameter for spacing near end joints shall be parallel to the longitudinal axis of the piece of lumber. The distance of knots from finger joints shall be measured from the edge of the knot nearest the joint to the closest part of the joint.

The grader must consider the end trim plus the length of the fingers, when determining if a knot will be in, or too close to, a finger joint.

3.4 Knotholes

Knotholes shall be permitted to be the same size as knots permitted in the grade. Other holes shall be permitted if no larger than the allowable knothole.

3.5 Splits and Shakes

Splits and shakes shall be permitted in all grades if extending from wide faces into the thickness of the piece at an angle of 45° or more from the wide face.

3.6 Checks

Seasoning checks are permitted.

3.7 Warp

Warp (including bow, crook and cup) shall not be so great that they will not be straightened out by pressure in bonding. Light crook shall be permitted.

3.8 Pitch Pockets and Streaks

Medium scattered pitch or bark pockets are permitted in all grades. Pitch streaks shall not exceed 1/6 of the width.

3.9 Torn Grain

Torn grain up to 1/16 inch shall be permitted with some occasional allowance for up to 1/8 inch.

3.10 Wane

Light wane which will be removed by resurfacing and therefore not be present in the finished timber shall be permitted at the time of grading. For specific combinations, wane not exceeding 1/6 the width on one or both edges of the wide face of a lamination, as permitted by the layup, shall be permitted in designated grades except that the outer laminations, shall be free of wane.

3.11 Slope of Grain

Slope of grain of visually graded lumber shall be limited in the full length of each lamination according to the appropriate grade and shall be measured over a distance sufficiently great to determine the general slope, disregarding local deviations, except as noted for special tension laminations.

3.12 Decay

Decay shall not be permitted, except that firm white speck in limited form may be allowed in some laminating grades as defined herein.

3.13 Timber Breaks

Timber breaks shall not be permitted.

3.14 Compression Wood

Compression wood in recognizable form shall be restricted in tension laminations up to 5% of the cross-section if neither damaging nor containing timber breaks. Other lamination grades have specific allowances per grade.

3.15 Saw kerfs

Saw kerfs shall not be allowed in the outer 5% of the member depth. Other zones shall be permitted to have saw kerfs equal to or less than one-half of the allowable knot size for the grade.

3.16 Growth Rate

Density of all species, if visually determined, shall be graded according to the following:

- (a) Dense (D): Dense lumber shall average not less than 6 annual rings per inch and 1/3 or more summerwood. Pieces averaging less than 6 annual rings per inch but not less than 4 are accepted as dense if averaging 1/2 or more summerwood.
- (b) Close (CL): Douglas-Fir-Larch only. Close grain lumber shall have a minimum average of 6 but no more than 30 annual rings per inch with no restriction on the percentage of summerwood. Pieces averaging 5 rings shall be accepted as close grain if averaging 1/3 or more summerwood.
- (c) Medium (M): Medium grain lumber shall have 4 or more annual rings per inch. In Douglas Fir, pieces averaging less than 4 rings per inch are accepted if averaging 1/3 or more summerwood. Medium grain is not defined in the current SPIB Standard Grading Rules, but is required for some laminating grades of southern pine.
- (d) Coarse (C): SP only. Coarse grain is that which fails to meet the requirements for medium grain. Coarse grain is not defined in the current SPIB Standard Grading Rules, but is permitted for some laminating grades of southern pine.

4. VISUAL GRADES

4.1 General Requirements

4.1.1 Knots

The knot sizes for structural laminating grades of western species are based on a fraction of the dressed width of the piece of lumber. The knot sizes for structural joists and planks and structural light framing grades of all species are tabulated on the basis of the nominal width.

Knots shall be well spaced. "Well spaced" means that the sum of all knots in any 6 inches of length of a piece shall not exceed twice the size of the largest knot permitted, and more than one knot of the maximum permissible size shall not be in the same 6 inches of length. Tension laminations shall be excluded from this rule due to more restrictive spacing requirements.

4.1.2 Slope of Grain

Slope of grain of visually graded lumber shall be limited in the full length of each lamination and shall be measured over a distance sufficiently great to determine the general slope, disregarding local deviations, except as noted for special tension laminations.

4.1.3 Density or Growth Rate

Growth rate shall be verified on both ends of visually graded tension laminations. In other visual grades, growth rate is permitted to be assessed by looking at one end of the piece only, except as noted for special tension laminations.

4.1.4 Specific Gravity of Species

Density or growth rate shall be permitted to be determined by weight using the method described in Section 7. When weight is used to establish growth rate, grades requiring dense rate of growth shall have a specific gravity above the near average specific gravity for the species as shown in the table below.

Species	Ave. SG at 12% MC
AC	0.42
DF-L	0.46
DF-S	0.50
HF	0.39
SP	0.49
SPF	0.35
SW	0.32

4.2 Laminating Grades

4.2.1 General

In general, laminating grades are designated with an "L," with the exception of southern pine (which uses "N"). The grade follows, then the density designation. Grades without density designations are considered medium. Example: L1D is laminating grade 1, dense.

4.2.2 Grade Specific Requirements

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

4.2.2.1 L1D

(a) Density: Dense.

Exception: "L1" for Douglas-Fir-Larch/Douglas-Fir South is considered dense. No density designation as per 4.2.2 is required.

- (b) Knot Size: Knots shall not occupy more than 1/4 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:14 for the full length of the piece.

4.2.2.2 L1

- (a) Density: Medium (except Douglas-Fir-Larch/Douglas-Fir South, which is dense).
- (b) Knot Size: Knots shall not occupy more than 1/4 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:14 for the full length of the piece.

4.2.2.3 L1CL

- (a) Density: Close.
- (b) Knot Size: Knots shall not occupy more than 1/4 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:12 for the full length of the piece.

4.2.2.4 L2D

- (a) Density: Dense.
- (b) Knot Size: Knots shall not occupy more than 1/3 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:12 for the full length of the piece
- (d) White Speck: Firm white specks are permitted. A combination of white speck and a knot in the same cross-section shall not occupy more than 1/3 the width or equivalent.

4.2.2.5 L2

- (a) Density: Medium.
- (b) Knot Size: Knots shall not occupy more than 1/3 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:12 for the full length of the piece.
- (d) White Speck: Firm white specks are permitted. A combination of white speck and a knot in the same cross-section shall not occupy more than 1/3 the width or equivalent.

4.2.2.6 L3

- (a) Density: Medium.
- (b) Knot Size: Knots shall not occupy more than 1/2 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:8 for the full length of the piece.
- (*d*) White Speck: Firm white specks are permitted. A combination of white speck and a knot in the same cross-section shall not occupy more than 1/2 the width or equivalent.

4.3 Species Specific Requirements—Douglas-Fir-Larch/Douglas-Fir South

Reference herein to Douglas-Fir-Larch shall apply to Douglas-Fir and Western Larch grown within the states of Wyoming, Montana, Idaho, Washington, Oregon and California, because the design values shown are based on a statistical analysis of the growth characteristics of the lumber from these sources.

Reference herein to Douglas-Fir South shall apply to Douglas-Fir grown within the states of Arizona, Colorado, Nevada, New Mexico and Utah because the design values shown are based on a statistical analysis of the growth characteristics of the lumber from these sources.

4.4 Species Specific Requirements—Hem-Fir

Reference herein to Hem-Fir species shall apply to any one or any combination of the following species: Western Hemlock, Pacific Silver Fir, Noble Fir, Grand Fir, California Red Fir and White Fir, including Hem-Fir grown in Canada.

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Sections 4.1 and 4.2, the following requirements apply for additional grades:

4.4.1 SSS

- (a) Density: Dense by weight measurement only.
- (b) Knot Size: Knots shall not occupy more than 1/10 of the cross-section.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:18 for the full length of the piece.

4.5 Species Specific Requirements—Softwoods

Reference herein to these species (SW) shall apply to any of the softwood species grown in the United States and Canada having an assigned modulus of elasticity (E) of 1,000,000 psi or more and design values in shear of 135 psi or more for No. 3 structural joists and planks grade based on 19% moisture content. The Softwood Species are those listed in *Standard Grading Rules for Western Lumber* of the Western Wood Products Association, the *Standard Grading Rules for West Coast Lumber* of the West Coast Lumber Inspection Bureau, *Standard Specifications for Grades of California Redwood Lumber* of the Redwood Inspection Service, *Standard Grading Rules for Northeastern Lumber* of the Northeastern Lumber Manufacturers Association or the *Standard Grading Rules for Canadian Lumber* of the National Lumber Grades Authority in Canada.

4.6 Species Specific Requirements—Southern Pine

Reference herein to "southern pine" shall apply to the four major species of southern pines: Loblolly, Longleaf, Shortleaf and Slash, as defined in the *Southern Pine Inspection Bureau Grading Rules* of the Southern Pine Inspection Bureau (SPIB).

The slope of grain for each grade is the maximum slope of grain allowed for the grade. Lamination requirements for the specified layup may be more restrictive than the basic slope of grain permitted by the grade. Where applicable, the more restrictive requirements apply. This standard (ANSI 117) specifies slope of grain requirements for a particular lamination.

4.6.1 N1D

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Dense.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:10 for the full length of the piece.
- (c) Knot Size:

Width (in.)	4	6	8	10	12
Edge Knot (in.)	1	1-1/2	2	2-1/2	3
Center Knot (in.)	1-1/2	2-1/4	2-3/4	3-1/4	3-3/4

4.6.2 N1M

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Medium.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:10 for the full length of the piece.
- (c) Knot Size:

Width (in.)	4	6	8	10	12
Edge Knot (in.)	1	1-1/2	2	2-1/2	3
Center Knot (in.)	1-1/2	2-1/4	2-3/4	3-1/4	3-3/4

4.6.3 N2D

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Dense.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:8 for the full length of the piece.
- (c) Knot Size:

Width (in.)	4	6	8	10	12
Edge Knot (in.)	1-1/4	1-7/8	2-1/2	3-1/4	3-3/4
Center Knot (in.)	2	2-7/8	3-1/2	4-1/4	4-3/4

4.6.4 N2M

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Medium.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:8 for the full length of the piece.
- (c) Knot Size:

Nidth (in.)	4	6	8	10	12
Edge Knot (in.)	1-1/4	1-7/8	2-1/2	3-1/4	3-3/4
Center Knot (in.)	2	2-7/8	3-1/2	4-1/4	4-3/4

4.6.5 N3M

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Medium.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:8 for the full length of the piece.
- (c) Knot Size:

Width (in.)	4	6	8	10	12
Edge Knot (in.)	1-3/4	2-3/4	3-1/2	4-1/2	5-1/2
Center Knot (in.)	2-1/2	3-3/4	4-1/2	5-1/2	6-1/2

4.6.6 N3C

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Section 4.1, the following requirements apply by grade:

- (a) Density: Coarse.
- (b) Slope of Grain: The basic slope of grain shall not exceed 1:4 for the full length of the piece.
- (c) Knot Size:

Width (in.)	4	6	8	10	12
Edge Knot (in.)	1-3/4	2-3/4	3-1/2	4-1/2	5-1/2
Center Knot (in.)	2-1/2	3-3/4	4-1/2	5-1/2	6-1/2

4.7 Grade Specific Requirements—Alaska Cedar

Reference herein to this species shall apply to Alaska Cedar grown in the United States or Canada.

In addition to the *General Requirements* outlined in Section 3, and the *General Requirements for Visual Grades* in Sections 4.1 and 4.2, the following additional requirements/exceptions apply by grade:

4.7.1 L1S

- (a) Density: Dense.
- (b) Knot Size: Knots shall not occupy more than 1/4 of the cross-section. A cross section shall be defined as any one-foot length.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:14 for the full length of the piece.

4.7.2 L1D

- (a) Density: Dense.
- **(b)** Knot Size: Knots shall not occupy more than 1/4 of the cross-section. A cross section shall be defined as any one-foot length.
- (c) Slope of Grain: The basic slope of grain shall not exceed 1:12 for the full length of the piece.

4.8 Grade Specific Requirements—California Redwood

Reference to this species herein applies to Redwood manufactured from timber grown within the Northern California coastal area as defined in the *Standard Specifications for Grades of California Redwood Lumber* of the Redwood Inspection Service. The design values shown herein are based on a statistical analysis of the growth characteristics of the lumber from this source.

Laminating lumber shall be of Redwood graded in accordance with the *Standard Specifications for Grades of California Redwood Lumber* of the Redwood Inspection Service.

There are five structural laminating grades of Redwood used for laminating purposes: "L1," clear all heart laminating; "L2," clear laminating; "L3," select heart laminating; "L4," construction heart laminating and "L5," construction laminating. See the above referenced standard for grading rules and specific requirements.

5. E-RATED GRADES (OTHER THAN 302 TENSION LAMINATIONS)

5.1 General

E-rated laminating lumber is lumber that has been selected by nondestructive measurement and by visual inspection for compliance with the grade stiffness and manufacturing requirements of Section 3. An E-rated laminating lumber grade includes pieces with edge characteristics (knots, knotholes, burls, distorted grain) up to the maximum size allowed for use with the grade in any laminated timber lay-up combination. E-rated lumber has additional visual restrictions for portions of the lumber not evaluated for stiffness.

5.2 Long-Span E (LSE)

Long-span E or LSE as defined herein shall be used as the standard nomenclature for specifying E values of E-rated laminating lumber.

5.2.1 Definition

Long-span E is defined as the Modulus of Elasticity (MOE) calculated from deflection measured in a flat-wise static bending test of lumber with center point loading and a span-depth ratio (l/d) of approximately 100.

5.2.2 Measurement

Long-span E shall be measured by the procedures of ASTM D4761, Bending Flatwise-Center Point Loading.

5.2.3 Lumber Production

E-rated laminating lumber shall be permitted to be produced with a system that measures MOE by means other than direct Long-span E measurement. Production equipment used to measure MOE shall be calibrated to produce E-rated laminating lumber grades meeting the Long-span E requirements of those grades. For purposes of calibration, Long-span E shall be measured by the procedures of ASTM D4761, *Bending Flatwise-Center Point Loading*.

5.3 E-Rated Laminating Lumber Specifications

5.3.1 Grade Names

E-rated laminating lumber grades shall be designated by the mean MOE of the grade, which is the mean Long-span E requirement of the grade, the word "LAM," and the denominator of allowable edge knot fraction. For example, a grade with a mean Long-span E requirement of 1,900,000 psi and an allowable 1/3 edge characteristic will be named "1.9E LAM-3." For reasons of spacing on a grade stamp, this is permitted to be shortened to 1.9E-3 on a stamp.

5.3.2 E Specifications for E-rated Lumber for Qualification

5.3.2.1 Mean Long-Span E

If the sample size is less than 125, the mean Long-span E of the lumber shall equal or exceed the specified grade mean MOE. Alternatively, if the sample size equals or exceeds 40, the mean Long-span E of the sample, E_t , shall meet the following criteria:

$$E_t \ge E_s - 1.303 (S_t / \sqrt{n_t})$$

where:

 S_t = the estimated population standard deviation (10⁶ psi)

 $S_t = (E_t - E_{st}) / 1.684 (10^6 \text{ psi})$

 n_t = sample size (≥ 40)

 E_t = mean Long-span E of the sample (10⁶ psi)

 E_s = grade Long-span E (10⁶ psi)

 E_{st} = 5th percentile Long-span E calculated from the test data (10⁶ psi)

5.3.2.2 MOE Distribution

The distribution of MOE values within an E-rated lumber grade shall be such that the 5th percentile value shall be equal to or greater than the grade 5th percentile values as shown in the table below.

Grade	Mean (10 ⁶ psi)	5th Percentile (106 psi)
2.6E LAM	2.6	2.26
2.5E LAM	2.5	2.16
2.4E LAM	2.4	2.06
2.3E LAM	2.3	1.96
2.2E LAM	2.2	1.86
2.1E LAM	2.1	1.77
2.0E LAM	2.0	1.67
1.9E LAM	1.9	1.58
1.8E LAM	1.8	1.48
1.7E LAM	1.7	1.39
1.6E LAM	1.6	1.30
1.5E LAM	1.5	1.21

5.3.3 Visual Limitations

5.3.3.1 Edge Characteristics

Characteristics such as knots, knotholes, burls, and distorted grain occurring at the edges of the wide faces shall be measured and limited to a fraction of the cross section in conformance with American Lumber Standards approved procedures in the following categories:

Edge Characteristics	Codes
1/6	6
1/4	4
1/3	3
1/2	2

5.3.3.2 Untested Portions

Portions of the lumber not tested by the E-rating device shall conform to the following visual limitations:

- (a) Non-Edge Knots equal to the largest non-edge knots in the tested portion of the piece or the next larger edge knot, whichever is greater.
- (b) Cross-Section Knots: Displacement of all knots in the same cross section shall not exceed the size of the permitted non-edge knot.
- (c) Slope of Grain: The general slope of grain in the untested portion shall not be steeper than:

Slope	Edge Characteristic (Disp.
1 in 12	1/6
1 in 10	>1/6 to ≤1/4
1 in 8	>1/4

5.4 Production Quality Control

5.4.1 Supervision

Quality control of E-rated laminating lumber shall be under the supervision of an accredited third-party inspection agency.

5.4.2 Quality Control

5.4.2.1 Formal Quality Control Program Required

A formal quality control program shall be maintained at the production facility to provide conformance to grade specifications on a continuous basis. The quality control program shall be approved by an accredited third-party inspection agency.

5.4.2.2 E-rated Grade Edge Characteristics

The edge characteristic restrictions applied for lay-up shall not be required to be considered when establishing the MOE criteria for quality control of an E-rated laminating lumber grade or when evaluating a given lot of E-rated laminating lumber for conformance to the E specifications of the grade of the lot.

5.4.2.3 Quality Control Records

Quality control records shall be maintained at the lumber production facility for a minimum of five (5) years.

5.5 Reinspection of Individual Lots for Conformance to Specifications

5.5.1 Test Method and Evaluation

The procedures of AITC Test T124 shall be used for testing and evaluating individual lots of E-rated laminating lumber for conformance to grade specifications.

5.5.2 Disposition of Nonconforming Lots

5.5.2.1 Regrade

The lumber shall be permitted to be regraded by testing all of the pieces in the lot in accordance with the Long-span E testing procedures of ASTM D4761, *Bending Flatwise-Center Point Loading*, and eliminating low E pieces from the lot so that the specifications for mean and lower 5th percentile E values of the E-rated grade are met. If the lumber is regraded by commercial testing devices other than a Long-span E measuring device, conformance to grade specifications shall be verified by AITC Test T124.

5.5.2.2 Assign a Lower Grade Level

The lumber shall be permitted to be used at a lower E-rated grade level for which the lot was qualified by the test results.

6. SPECIAL TENSION LAMINATION GRADES

6.1 General

There are six (6) grades of tension laminations, 302-20, 302-22, 302-24, 302-26, 302-28 and 302-30. The following general restrictions and limiting provision apply to all grades and sizes of lumber graded as tension laminations:

6.1.1 Cross Section

A one-foot length of a lamination shall be considered as a cross section.

6.1.2 Density

Growth rate requirements shall apply to the full length of the piece. All tension laminations shall be dense. Each piece shall have a specific gravity greater than the near average specific gravity for the species. See Section 4.1.4 for the near average specific gravity by species.

Exception: Certain exceptions apply as shown in the Alternate Rules for each grade below.

6.2 302-20

6.2.1 Primary Rules (All Species)

6.2.1.1 General

In addition to the basic requirements of the grades tabulated in these specifications, the following limitations shall apply to all 302-20 grades under the primary rules of grading:

- (a) Knots shall not occupy more than 1/4 of the width in any cross section.
- **(b)** The general slope of grain shall not be steeper than 1:12. Where more restrictive slope of grain is required by the laminating combinations, the more restrictive slope of grain shall apply.
- (c) Any cross-section shall have at least 50% clear wood free of strength-reducing characteristics with a slope of grain no steeper than 1:12. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/2 of the cross-section.

6.2.1.2 Visually Graded Combinations

In addition to the provisions in Section 6.2.1.1, the following applies to visually graded combinations:

(a) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross section shall be excluded. The next inch of wood outside the area of the pith-associated wood shall be dense. The line along which measurement of this inch is made shall correspond to the line used in the standard grading rules for rate of growth and percentage of summerwood. If a distance of one inch is not available along this line, the measurement will be made over such lesser portion as exists.

6.2.1.3 E-Rated Combinations

In addition to the provisions in Section 6.2.1.1, the following applies to E-rated combinations:

- (a) Laminations for E-rated combinations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension laminations.
- (b) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross section shall be excluded. All wood not included as pith-associated wood shall be at least medium grain rate of growth

6.2.2 Alternate Rules

6.2.2.1 Douglas-Fir-Larch

Exceptions to provisions in Section 6.2.1 are allowed for Douglas-Fir-Larch 302-20 tension laminations as follows. Provisions not listed here are not excepted:

(a) Knots shall not exceed the size listed in the following chart:

Nominal width, in.	4	6	8	10	12
Knot size, in.	3/8	1/2	3/4	7/8	1

- (b) Any cross-section shall have at least 3/4 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/4 of the cross section.
- (c) Slope of grain shall not be steeper than 1:10.
- (d) Pieces shall have a specific gravity of 0.45 or above based on oven-dried weight and volume at 12% moisture content.
- (e) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:10. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.

6.2.2.2 E-Rated

The following are alternative provisions for E-rated tension laminations. Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension laminations, except where specifically modified in this section. Lumber shall be from an E-rating system which employs continuously measured lowest point modulus of elasticity. In addition to these basic requirements the following limitations shall apply:

- (a) Centerline knots shall not occupy more than 1/4 of the cross section.
- (b) Edge knots are limited to that allowed by the E-rated grade.
- (c) Special Provisions for Ends of Piece: In addition to the visual requirements above, the untested portion(s) of each piece shall be visually graded to meet the following:
 - 1. The untested portion(s) of the piece shall have the same general character as the remainder of the piece.
 - **2.** The general slope of grain shall not be steeper than 1:12.
 - 3. Any cross-section shall have at least 1/2 clear wood free of strength reducing characteristics.
- (d) Testing Provisions: When this alternative provision is used the lumber shall be tested and qualified in accordance with AITC Test T123. Criteria for acceptance shall be that the 5th percentile with 75% confidence determined by AITC Test T123 shall equal or exceed 3,340 psi.
- (e) Application: Tension laminations qualified under this alternate provision are permitted to be used for all visually graded combinations without regard to the Long-span E provided the compression perpendicular to grain design values are satisfied.

6.3 302-22

6.3.1 Primary Rules (All Species)

6.3.1.1 General

In addition to the basic requirements of the grades tabulated in these specifications, the following limitations shall apply to all 302-22 grades under the primary rules of grading:

- (a) Knots shall not occupy more than 1/4 of the width in any cross-section.
- (b) Any cross-section shall have at least 60% clear wood free of strength-reducing characteristics with a slope of grain no steeper than 1:16. Knots plus associated localized cross grain, or knots plus associated localized cross grain plus associated cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 40% of the cross-section.
- (c) The general slope of grain shall not be steeper than 1:16. Where more restrictive slope of grain is required by the laminating combinations, the more restrictive slope of grain shall apply.

6.3.1.2 Visually Graded Combinations

In addition to the provisions in Section 6.3.1.1, the following applies to visually graded combinations:

(a) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross-section shall be excluded. The next inch of wood outside the area of the pith-associated wood shall meet the growth rate requirements of the grade, including "dense" when dense laminations are required. The line along which measurement of this inch is made shall correspond to the line used in the standard grading rules for rate of growth and percentage of summerwood. If a distance of one inch is not available along this line, the measurement will be made over such lesser portion as exists.

6.3.1.3 E-Rated Combinations

In addition to the provisions in Section 6.3.1.1, the following applies to E-rated combinations:

- (a) Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension laminations.
- (b) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross section shall be excluded. All wood not included as pith-associated wood shall be of at least medium grain rate of growth.

6.3.2 Alternate Rules

6.3.2.1 Douglas-Fir-Larch

Exceptions to provisions in Section 6.3.1 are allowed for Douglas-Fir-Larch 302-22 tension laminations as follows. Provisions not listed here are not excepted:

(a) Knots shall not exceed the size listed in the following chart:

Nominal width, in.	4	6	8	10	12
Knot size, in.	3/8	1/2	3/4	7/8	1

- (b) Any cross-section shall have at least 3/4 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/4 of the cross section.
- (c) Slope of grain shall not be steeper than 1:16.
- (d) Growth rate requirements shall apply to the full length of the piece. Douglas-Fir-Larch tension laminations are required to have at least an average of six annual rings per inch. Pieces shall have a specific gravity of 0.35 or above based on oven-dried weight and volume of 12% moisture content. This tension lamination provides a compression perpendicular to grain design value of 590 psi. Where required to have 650 psi compression perpendicular to grain design value, at least one dense two inch nominal thickness lamination is required in the bearing area.
- (e) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:16. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.

6.3.2.2 Douglas-Fir-Larch

Exceptions to provisions in Section 6.3.1 are allowed for Douglas Fir-Larch 302-22 tension laminations as follows. Provisions not listed here are not excepted:

(a) Knots shall not exceed the size listed in the following chart:

Nominal width, in.	4	6	8	10	12
Knot size, in.	3/8	1/2	3/4	7/8	1

- (b) Any cross-section shall have at least 3/4 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/4 of the cross section.
- (c) Slope of grain shall not be steeper than 1:12.
- (d) Growth rate requirements shall apply to the full length of the piece. Douglas-Fir-Larch tension laminations are required to have at least an average of 6 annual rings per inch. This tension lamination provides a compression perpendicular to grain design value of 590 psi. Where required to have 650 psi compression perpendicular to grain design value, at least one dense two inch nominal thickness lamination is required in the bearing area.
- (e) The long-span modulus of elasticity shall not be less than 1,700,000 psi.
- (f) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:12. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.

6.3.2.3 E-rated

The following are alternative provisions for E-rated tension laminations. Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension lamination, except where specifically modified in this section. Lumber shall be from an E-rating system which employs continuously measured lowest point modulus of elasticity. In addition to these basic requirements the following limitations shall apply:

- (a) Centerline knots shall not occupy more than 1/4 of the cross section.
- **(b)** Edge knots are limited to that allowed by the E-rated grade.
- (c) Special Provisions for Ends of Piece: In addition to the visual requirements above, the untested portion(s) of each piece shall be visually graded to meet the following:
 - 1. The untested portion(s) of the piece shall have the same general character as the remainder of the piece.
 - **2.** The general slope of grain shall not be steeper than 1:12.
 - 3. Any cross-section shall have at least 60% clear wood free of strength reducing characteristics.
- (d) Testing Provisions: When this alternative provision is used the lumber shall be tested and qualified in accordance with AITC Test T123. Criteria for acceptance shall be that the 5th percentile with 75% confidence determined by AITC Test T123 shall equal or exceed 3,670 psi.
- (e) Application: Tension laminations qualified under this alternate provision are permitted to be used for all visually graded combinations without regard to the Long-span E provided the compression perpendicular to grain design values are satisfied.

6.4 302-24

6.4.1 Primary Rules

6.4.1.1 General

In addition to the basic requirements of the grades tabulated in these specifications, the following limitations shall apply to all 302-24 grades under the primary rules of grading:

- (a) Knots shall not occupy more than 1/5 of the width in any cross section.
- (b) Any cross-section shall have at least 2/3 clear wood free of strength-reducing characteristics with a slope of grain no steeper than 1:16. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/3 of the cross-section.
- (c) Maximum size single strength-reducing characteristics when not in the same horizontal projection shall be at least two feet apart measured center to center.
- (*d*) The general slope of grain shall not be steeper than 1:16. Where more restrictive slope of grain is required by the laminating combinations, the more restrictive slope of grain shall apply.

6.4.1.2 Visually Graded Combinations

In addition to the provisions in Section 6.4.1.1, the following applies to visually graded combinations:

(a) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross section shall be excluded. The next inch of wood outside the area of the pith-associated wood shall meet the growth rate requirements of the grade, including "dense" when dense laminations are required. The line along which measurement of this inch is made shall correspond to the line used in the standard grading rules for rate of growth and percentage of summerwood. If a distance of one inch is not available along this line, the measurement will be made over such lesser portion as exists.

6.4.1.3 E-Rated Combinations

In addition to the provisions in Section 6.4.1.1, the following applies to E-rated combinations:

- (a) Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension lamination.
- (b) Pieces containing wide-ringed or lightweight pith-associated wood at the ends of the piece occupying over 1/8 of the cross section shall be excluded. All wood not included as pith-associated wood shall be at least medium grain rate of growth.

6.4.2 Alternate Rules

6.4.2.1 Douglas-Fir-Larch

Exceptions to provisions in 6.4.1 are allowed for Douglas-Fir-Larch 302-24 tension laminations as follows. Provisions not listed here are not excepted:

(a) Knots shall not exceed the size listed in the following chart:

Nominal width, in.	4	6	8	10	12
Knot size, in.	3/8	1/2	3/4	7/8	1

- (b) Any cross-section shall have at least 3/4 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/4 of the cross-section.
- (c) Maximum size single strength-reducing characteristics when not in the same horizontal projection shall be as least 2 feet apart measured center to center.
- (d) Slope of grain shall not be steeper than 1:12.
- (e) The long-span modulus of elasticity shall not be less than 1,800,000 psi.
- (f) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:12. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.

6.4.2.2 E-rated

The following are alternative provisions for E-rated tension laminations. Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade shown for the outer tension lamination, except where specifically modified in this section. Lumber shall be from an E-rating system which employs continuously measured lowest point modulus of elasticity. In addition to these basic requirements the following limitations shall apply:

- (a) Centerline knots shall not occupy more than 1/5 of the cross section.
- (b) Maximum size single strength-reducing characteristics when not in the same horizontal projection shall be at least two feet apart measured center to center.
- (c) Edge knots are limited to that allowed by the E-rated grade.
- (*d*) **Special Provisions for Ends of Piece:** In addition to the visual requirements above, the untested portion(s) of each piece shall be visually graded to meet the following:
 - 1. The untested portion(s) of the piece shall have the same general character as the remainder of the piece.
 - **2.** The general slope of grain shall not be steeper than 1:12.
 - 3. Any cross-section shall have at least 2/3 clear wood free of strength-reducing characteristics.
- (e) **Testing Provisions:** When this alternative provision is used the lumber shall be tested and qualified in accordance with AITC Test T123. Criteria for acceptance shall be that the 5th percentile with 75% confidence determined by AITC Test T123 shall equal or exceed 4,000 psi.
- (f) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:12. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.
- (g) Application: Tension laminations qualified under this alternate provision are permitted to be used for all visually graded combinations without regard to the Long-span E provided the compression perpendicular to grain design values are satisfied.

6.5 302-26

6.5.1 Primary Rules

In addition to the basic requirements of the 302-24 lamination grade as tabulated in Section 6.4, the following limitations shall apply:

(a) Any cross-section containing an edge knot shall have 80% clear and straight-grained wood.

6.6 302-28

6.6.1 Primary Rules

In addition to the basic requirements of the 302-24 lamination grade as tabulated in Section 6.4, the following limitations shall apply:

(a) Average Long-span E for the grade shall be 2.3×10^6 psi with no piece less than 1.96×10^6 psi and shall be verified through daily quality control.

6.7 302-30

6.7.1 Primary Rules

In addition to the basic requirements of the 302-26 lamination grade as tabulated in Section 6.5, the following limitations shall apply:

(a) Average Long-span E for the grade shall be 2.3×10^6 psi with no piece less than 1.96×10^6 psi and shall be verified through daily quality control.

6.8 Alternate Rules by Species

6.8.1 Southern Pine

Exceptions to provisions in Sections 6.2, 6.3 and 6.4 are allowed for southern pine as follows. Provisions not listed here are not excepted:

(a) Knots shall not exceed the size listed in the following chart:

Nominal width, in.	4	6	8	10	12
Knot size, in.	3/8	1/2	3/4	7/8	1

- **(b)** Any cross-section shall have at least 3/4 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, or knots plus associated localized cross grain not associated with a knot, or localized cross grain not associated with a knot is permitted to occupy up to 1/4 of the cross-section.
- (c) Slope of grain shall be no steeper than 1:10 for 302-20 and 1:12 for 302-22 and 302-24.
- (d) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up the maximum allowable for said grade. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.

6.8.2 E-Rated Hem Fir

The following are alternative provisions to those included in Sections 6.1, 6.2 and 6.3 for E-rated Hem-Fir tension laminations:

- (a) Laminations shall be visually graded and E-rated in accordance with all of the requirements for the E-rated grade tabulated in these specifications for the outer tension lamination except where specifically modified in this section.
- (b) Laminations shall conform to WCLIB Standard No. 17, paragraph 101-c, except that the 3-inch cutout provision does not apply.
- (c) The knot size permitted for all widths is a small knot (3/4-inch diameter). The number of 3/4-inch knots permitted is proportionate to the size of the piece of lumber in accordance with paragraph 101-c of WCLIB Standard No. 17.
- (d) The 1/6th edge knot characteristic restriction shall be applied to nominal 4-inch wide lumber. For 302-24, 2.0E-1/6 grade is required, for 302-22, 1.8E-1/6 grade is required and for 302-20, 1.5E-1/4 grade is required.

- (e) Any cross-section shall have at least 2/3 clear wood free of strength-reducing characteristics. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot are permitted to occupy up to 1/3 of the cross-section.
- (f) Slope of grain shall be no steeper than 1:12.
- (g) For 302-24 grade, maximum size single strength-reducing characteristics when not in the same horizontal projection shall be at least two feet apart measured center to center.
- (h) Special Provisions for Ends of Piece: The untested portion of each end of each piece shall be visually graded to meet the following:
 - 1. The ends of the piece shall have the same general character as the remainder of the piece.
 - **2.** Any cross-section shall have at least 1/2, 3/5 or 2/3 clear wood free of strength-reducing characteristics for 302-20, 302-22 or 302-24 respectively. Knots plus associated localized cross grain, knots plus associated localized cross grain plus localized cross grain not associated with a knot, or localized cross grain not associated with a knot are permitted to occupy up to 1/2, 2/5 or 1/3 of the cross-section for 302-20, 302-22 and 302-24, respectively.
- (i) End Joint Qualification: Manufacturers using these alternative tension lamination provisions shall qualify their end joint by testing 30 end joints containing the maximum slope of grain to be used in the plant for this grade up to 1:12. Test procedures and criteria for acceptance of this test are as contained in ASTM D7469 and ANSI A190.1.
- (j) Testing Provisions: The provisions for end joint qualification for clear wood at a cross-section and general slope of grain is permitted to be eliminated if a test is conducted in accordance with AITC Test T123 to verify the strength of lumber from the E-rating system which employs continuously measured lowest point modulus of elasticity. Criteria for acceptance shall be that the 5th percentile with 75% confidence determined by AITC Test T123 shall equal or exceed the following values:

Grade	Test Value at 5th Percentile, psi
302-24	4,000
302-22	3,670
302-20	3,340

6.9 C-14: Alternate Provision for Machine-Graded Tension Laminations

6.9.1 General

This alternate provision covers lumber mechanically graded under the provisions of the American Lumber Standard (ALS). These grades shall be qualified and quality controlled by test for strength and stiffness by an agency qualified by ALS. These grades include machine stress-rated lumber (MSR) and machine-evaluated lumber (MEL). Machine-graded lumber is lumber manufactured with the use of grading methodologies that include the use of machines for identifying mechanical properties in the grading process. This alternate provision shall be applied to lumber from each machine grading facility and grading system seeking qualification for production of tension laminations to be used on structural glued laminated timber, with grades equivalent to the 302-20, 302-22 and 302-24 grades required. Machine-graded lumber to be used under this alternate

provision shall meet specific product descriptions as defined in the various standards. Qualification records shall be maintained at the facility where carried out and shall be available for review by the accredited third-party inspection agency of the laminator.

Lumber to be qualified for tension laminations under this alternate provision shall be manufactured by a facility qualified to produce machine-graded lumber under the supervision of a grading agency accredited by the American Lumber Standards Committee. This grading practice shall meet the quality control provision of such a grading agency and include quality control for tensile strength and Long-span E properties.

6.9.2 Visual Grading

The general visual requirements for machine-graded lumber plus any additional visual limitations required by the supervisory grading agency for qualification under the provisions shall apply. In addition, the general lumber requirements contained in Section 3 shall apply.

6.9.3 Special Visual Grading Requirements

The supervisory grading agency shall provide appropriate visual limitations applicable to those portions of pieces not subjected to machine grading which will assure that the tensile strength requirements of the grade are maintained. For this purpose, these rules are permitted to be those applied in Sections 6.2, 6.3 and 6.4 to obtain grades equivalent to 302-20, 302-22 and 302-24.

6.9.4 Quality Control

The quality control requirements of this alternate tension lamination material are the responsibility of the lumber producer under the supervision of a grading agency accredited by the American Lumber Standards Committee. Records for the respective quality control responsibilities shall be maintained at the facility where carried out and shall be available for periodic review by the lumber grading agency and the accredited third-party inspection agency of the laminator.

If the lumber is supplied to the laminator as meeting the requirements of Sections 2, 6.7.1 and 6.7.2, all mechanical and visual inspection and quality control requirements shall be the responsibility of the machine grading facility.

If lumber is supplied to the laminator as meeting only the mechanical and visual stress grading criteria of Section 6.7.1, those inspection and quality control requirements shall be the responsibility of the machine grading facility; however, the laminator shall be responsible for the additional visual grading required to meet the laminating criteria of this standard.

6.9.5 Identification

Each piece of machine-graded lumber used under this alternative provision shall be grade stamped with the appropriate stamp of the supervisory lumber grading agency.

6.9.6 Changes in Practice

If, in the judgment of the accredited third-party inspection agency of the laminator, significant changes are made in the visual or machine grading practice, the qualification prescribed herein shall be invalid and shall be re-qualified.

6.9.7 Testing Provisions

When this alternative provision is used, the lumber shall be qualified for tensile strength and Long-span E using a sample size of not less than 102 pieces. The testing procedures of AITC Test T123 shall be used for testing tensile properties. The testing procedures of ASTM D4761, Bending Flatwise-Center Point Loading, shall be used for testing Long-span E.

6.9.8 Criteria for Acceptance

6.9.8.1 Tensile Strength Qualification

For qualification for a tension lamination grade, the 5th percentile tensile strength estimated with 75 percent confidence shall equal or exceed the values calculated as follows:

Grade	Test Value at 5th Percentile, psi
302-24	4,000
302-22	3,670
302-20	3,340

Tension laminations for beams 6 inches or less in width and greater than 15 inches in depth shall meet or exceed 1.67 times the beam design value in bending, Fbx. The values established in this way are then adjusted for lamination width by multiplying by the factors of 0.95, 0.90 and 0.84 for nominal 8, 10 and 12 inches widths respectively. These values are then reduced for beams of lesser depth by multiplying by factors of 0.90 for beams 12 inches to 15 inches in depth and 0.80 for beams less than 12 inches in depth.

6.9.8.2 End Joint Qualification

Manufacturers using tension laminations qualified under this alternative provision shall qualify the end joints by following procedures in ASTM D7469 by testing 30 end joints in tension made from representative lumber from the machine-grading system.

6.9.9 Application

Tension laminations qualified under this alternative provision are permitted to be used for all visually graded and E-rated combinations provided the average Long-span E of the laminations is at least equal to the average Long-span E of the grade of lumber for which it is being substituted and the compression perpendicular to grain design values are satisfied.

6.9.10 Reinspection and Testing of Individual Lots for Conformance to Specifications

The procedures of the grading agency supervising the production of the lumber shall be used for re-inspecting individual lots for conformance to specifications.

6.9.11 Records

The grading agency that supervises qualification to the provisions of C14 shall report a summary of the qualification results to the accredited third-party inspection agency of the laminator.

7. METHOD FOR DETERMINATION OF SPECIFIC GRAVITY

7.1 General

Measuring specific gravity of a piece of lumber shall be permitted to be used to determine density for all softwood species used for laminating, and shall be required to be used for dense Hem-Fir, since ring count and percent summerwood do not provide a reliable measure of density for Hem-Fir.

In determining specific gravity, lumber is weighed and a weight per volume is calculated. From this number the specific gravity can be calculated. In weighing lumber to determine specific gravity, several factors shall be taken into account: moisture content of the lumber; width, thickness and length; and accuracy of the measurements.

7.2 Moisture Content

Moisture contents shall be measured with a moisture meter calibrated for the species being tested. The moisture content of lumber at the time of weighing shall be taken into account in determining whether or not a piece meets the minimum weight requirements for the species. The range of moisture content of lumber used for laminating is relatively small. However, in the preparation of charts to use in production, the minimum weights for 8%, 12% and 16% moisture content are recommended. Minimum weights for intermediate moisture contents may be interpolated.

7.3 Size

The thickness and width of lumber shall be maintained according to ANSI A190.1 tolerances, and measured to the nearest 0.01 inch at the time of weighing. Length shall be measured to the nearest 1/8 inch.

7.4 Method of Weighing

Any method of weighing the nearest 0.01 lbf is satisfactory.

7.5 Calculation of Specific Gravity

Calculation of specific gravity shall be normalized to 12% moisture content in order to compare it to the required levels. ASTM D2395 shall be used to calculate specific gravity.

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- 9. ASTM. 2012. Standard D3737. Standard Practice for Establishing Allowable Properties for Structural Glued Laminated Timber (Glulam). ASTM International. West Conshohocken, Pennsylvania.
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