

# **ICC-ES Evaluation Report**

## **ESR-5752**

Reissued May 2025

This report also contains:

- City of LA Supplement

Subject to renewal May 2026

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DIVISION: 06 00 00— WOOD, PLASTICS AND COMPOSITES

Section: 06 02 00— Design Information

Section: 06 18 13— Glued-Laminated Beams REPORT HOLDER: ROSBORO COMPANY, EVALUATION SUBJECT:
GLUED-LAMINATED
TIMBER



# 1.0 EVALUATION SCOPE

# Compliance with the following codes:

- 2024, 2021, 2018, 2015 and 2012 *International Building Code*® (IBC)
- 2024, 2021, 2018, 2015 and 2012 *International Residential Code*® (IRC)

# Property evaluated:

■ Structural

# **2.0 USES**

The Rosboro structural glued-laminated timbers (glulams) are used as structural components, such as beams, columns, decking, and rim boards, in buildings where Types III, IV, IV-HT, and V construction is permitted by building codes.

# 3.0 DESCRIPTION

- **3.1 General:** The glulam products recognized in this report are manufactured by Rosboro Company in accordance with ANSI A190.1 based on layup combinations published in ANSI 117 or developed in accordance with ASTM D7341. Individual beam laminations are 2 inches (51 mm) or less in net thickness. Beam widths are between 2 ½ and 10 inches (64 and 254 mm), and beam depths are 6 inches (235 mm) or deeper.
- **3.2** Adhesive: Face and end-joint bonding adhesives comply with ASTM D2559 for exterior or wet use.
- **3.3 End Joints:** End joints comply with ANSI A190.1.
- **3.4 Laminating Lumber:** Rosboro glulams are manufactured using visually graded or E-rated lumber laminations that comply with rules of applicable approved lumber grading agencies and the procedures specified in the manufacturer's quality control manual in accordance with ANSI 117 and ANSI A190.1. Quality control for E-rating is conducted under the supervision of an approved third-party inspection agency.
- **3.5 Layup Combinations:** Rosboro glulams are fabricated in accordance with ANSI A190.1 using the mixed-grade combinations noted in <u>Table 1</u> or single-grade combinations noted in <u>Table 2</u> of this report. Resawn purlin beams, manufactured by ripping nominally 6-inch beams vertically through their depth into two members of equal width, are permitted in accordance with ANSI A190.1.

# 4.0 DESIGN

Rosboro glulams described in this evaluation report comply with the building codes and are permitted to be designed in accordance with the National Design Specification for Wood Construction (NDS) or ANSI 117 using the allowable stress design (ASD) properties published in <u>Tables 1</u> and <u>2</u>. Design values for the Load and Resistance Factor Design (LRFD) shall be permitted to be converted from the ASD values using the format conversion factors provided in Appendix N of the NDS.

# **5.0 CONDITIONS OF USE:**

The specific glulam combinations described in this report comply with or are suitable alternatives to what is specified in those codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 Fabrication, design, and installation must comply with this evaluation report and the manufacturer's published design/installation instructions, and the applicable code. In the event of a conflict between this evaluation report and the manufacturer's design/published installation instructions, the most restrictive one governs.
- 5.2 The manufacturer's design and/or installation instructions must be available at the jobsite at all time during installation.
- **5.3** ASD referenced design values for normal conditions of loading must not exceed those provided in Tables 1 and 2.
- **5.4** ASD referenced design values for combinations noted in <u>Table 1</u> are for members with four or more laminations stressed primarily in bending due to loads applied perpendicular to the wide faces of the laminations. Referenced design values are included, however, for axial stresses and stresses from bending due to loads applied parallel to the wide faces of the laminations.
- **5.5** ASD referenced design values for combinations noted in <u>Table 2</u> are for members with two or more laminations stressed primarily axially or in bending due to loads applied parallel to the wide faces of the laminations. Referenced design values are included, however, for stresses from bending due to loads applied perpendicular to the wide faces of the laminations.
- **5.6** Design calculations, signed and sealed by a registered design professional, verifying compliance with this report and the design requirements of the applicable code, must be submitted to the code official for approval.
- 5.7 The effects of checking on the glulam members are outside the scope of this report.
- 5.8 Rosboro glulams are manufactured under a quality assurance program with inspections by ICC-ES.

# **6.0 EVIDENCE SUBMITTED**

- **6.1** Data in accordance with ANSI 117, ANSI A190.1, and ANSI 405.
- **6.2** Data in accordance with ASTM D198, ASTM D2559, and ASTM D3737.
- **6.3** Quality documentation.

## 7.0 IDENTIFICATION

- **7.1** The ICC-ES mark of conformity, electronic labeling, or the evaluation report number (ICC-ES ESR-5752) along with the name, registered trademark, or registered logo of the report holder (Rosboro Company, LLC) must be included in the product label.
- **7.2** In addition, Rosboro glulams are identified by a stamp bearing the manufacturing plant number or address, the glulam combination identification symbol, and the name of the inspection agency.
- **7.3** The report holder's contact information is the following:

ROSBORO COMPANY, LLC 2509 MAIN STREET SPRINGFIELD, OREGON 97477 (541) 746-8411 https://rosboro.com/



# TABLE 1– REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATEDTIMBER<sup>(a,b)</sup> (MEMBERS STRESSED PRIMARILY IN BENDING)

Combination Symbol	Species <sup>(c)</sup> Outer/Core (Bal or Unbal <sup>(d)</sup> )	Bending About X-X Axis (Loaded Perpendicular to Wide Faces of Laminations)								Bending About Y-Y Axis (Loaded Parallel to Wide Faces of Laminations)							Axially Loaded		Fasteners	
		Extreme Fiber in Bending <sup>(e)</sup>		Compression Perpendicular to Grain		Shear				Extreme	Compression	Shear				Tension	O	Specific Gravity for Fastener Design		
		Bottom of Beam Stressed in tension (Positive Bending)	Top of Beam Stressed in Tension (Negative Bending)	Tension Face	Compression Face	Parallel to Grain	Modulus of Elasticity <sup>(h)</sup>			Fiber in Bending <sup>(i)</sup>	Perpendicular to Grain	Parallel to Grain	Modulus of Elasticity <sup>(h)</sup>			Parallel to Grain	Compression Parallel to Grain	Top or Bottom Face	Side Face	
		F <sub>bx</sub> + (psi)	F <sub>bx</sub> - (psi)		F <sub>c1x</sub> (psi)	F <sub>vx</sub> <sup>(f)</sup> (psi)	E <sub>x true</sub> (10 <sup>6</sup> psi)	E <sub>x app</sub> (10 <sup>6</sup> psi)	<b>E</b> <sub>x min</sub> (10 <sup>6</sup> psi)	F <sub>by</sub> (psi)	F <sub>с⊥у</sub> (psi)	F <sub>vy</sub> <sup>(f,g)</sup> (psi)	E <sub>y true</sub> (10 <sup>6</sup> psi)	E <sub>y app</sub> (10 <sup>6</sup> psi)	<b>E</b> <sub>y min</sub> (10 <sup>6</sup> psi)	F <sub>t</sub> (psi)	F <sub>c</sub> (psi)	G	j	
16F-V3	DF/DF (U)	1600	1250	560	560	265	1.6	1.5	0.79	1450	560	230	1.6	1.5	0.79	975	1500	0.50	0.50	
20F-V3 20F-V7 20F-V12 20F-V13	DF/DF (U) DF/DF (B) AC/AC (U) AC/AC (B)	2000 2000 2000 2000	1450 2000 1400 2000	650 650 560 560	560 650 560 560	265 265 265 265	1.7 1.7 1.6 1.6	1.6 1.6 1.5 1.5	0.85 0.85 0.79 0.79	1450 1450 1250 1250	560 560 470 470	230 230 230 230	1.6 1.7 1.5 1.5	1.5 1.6 1.4 1.4	0.79 0.85 0.74 0.74	1000 1050 925 950	1550 1600 1500 1550	0.50 0.50 0.46 0.46	0.50 0.50 0.46 0.46	
24F-V4 24F-V4-2.0Etrue 24F-V5 24F-V8 24F-V8-2.0Etrue 24F-V10	DF/DF (U) DF/DF (U) DF/HF (U) DF/DF (B) DF/DF (B) DF/HF (B)	2400 2400 2400 2400 2400 2400 2400	1850 1850 1600 2400 2400 2400	650 650 650 650 650 650	650 650 650 650 650 650	265 265 215 265 265 215	1.9 2.0 1.8 1.9 2.0 1.9	1.8 1.9 1.7 1.8 1.9	0.95 1.00 0.90 0.95 1.00 0.95	1450 1450 1350 1550 1550 1450	560 560 375 560 560 375	230 230 200 230 230 230	1.7 1.8 1.6 1.7 1.8 1.6	1.6 1.7 1.5 1.6 1.7	0.85 0.90 0.79 0.85 0.90 0.79	1100 1100 1100 1100 1100 1150	1650 1650 1450 1650 1650 1550	0.50 0.50 0.50 0.50 0.50 0.50	0.50 0.50 0.43 0.50 0.50 0.43	
24F-V1 24F-V5	SP/SP (U) SP/SP (B)	2400 2400	1750 2400	740 740	650 740	300 300	1.8 1.8	1.7 1.7	0.90 0.90	1450 1700	650 650	260 260	1.6 1.7	1.5 1.6	0.79 0.85	1100 1150	1500 1600	0.55 0.55	0.55 0.55	
30F-E2M3 <sup>(k)</sup> 30F-E/DF2 <sup>(k)</sup>	LVL/SP (B) LVL/DF (B)	3000 3000	3000 3000	650 <sup>(l)</sup>	650 <sup>(l)</sup> 650 <sup>(l)</sup>	300 265 <sup>(m)</sup>	2.2 2.2	2.1 2.1	1.11 1.11	1750 1550	650 560	260 230	1.8 1.8	1.7 1.7	0.90 0.90	1350 1100	1750 1650	0.50 0.50	0.50 0.50	
Wet-use factors		0.8		0.53		0.875	0.833		0.8	0.8 0.53 0.875		0.833			8.0	0.73	See N	NDS		

#### For SI: 1 psi = 6.895 Pa

- (a) The combinations in this table are applicable to members consisting of 4 or more laminations and are intended primarily for members stressed in bending due to loads applied perpendicular to the wide faces of the laminations. However, design values are tabulated for loading both perpendicular and parallel to the wide faces of the laminations. For combinations and design values applicable to members loaded primarily axially or parallel to the wide faces of the laminations, see <u>Table 2</u>.
- (b) The tabulated design values are for normal duration of loading. For other durations of loading, see applicable building code. The tabulated design values are for dry conditions of use. For wet conditions of use, multiply the tabulated values by the factors shown at the bottom of the table.
- (c) The symbols used for species are AC = Alaska cedar, DF = Douglas fir-larch, HF = Hem-fir, SP = Southern pine, and LVL = Laminated veneer lumber in accordance with the manufacturing standard.
- (d) The unbalanced (U) layup is intended primarily for simple-span applications and the balanced (B) layup is intended primarily for continuous or cantilevered applications.
- (e) The tabulated design values in bending,  $F_{bx}$ , are based on members  $5^{1}/_{8}$  inches in width by 12 inches in depth by 21 feet in length. For members with a larger volume,  $F_{bx}$  must be multiplied by a volume factor,  $Cv = (5.125/b)^{1/x} (12/d)^{1/x}$  ( $(21/L)^{1/x}$ , where b is the beam depth (in.), L is the beam length between the points of zero moment (ft), and x = 20 for Southern pine or x = 10 for other species. The tabulated  $F_{bx}$  values require the use of special tension laminations. If these special tension laminations are omitted, the  $F_{bx}$  values must be multiplied by 0.75 for members greater than or equal to 15 inches or by 0.85 for members less than 15 inches in depth.
- (f) The design values for shear,  $F_{vx}$  and  $F_{vy}$  shall be decreased by multiplying by a factor of 0.72 for non-prismatic members, notched members, and for all members subject to impact or cyclic loading. The reduced design value shall be used for the design of members at connections that transfer shear by mechanical fasteners. The reduced design value shall also be used for determining design values for the radial tension and torsion.  $F_{vx}$  and  $F_{wy}$  values do not include adjustments for checking.
- (g) Design values for  $F_w$  are for timber with laminations made from a single piece of lumber across the width or multiple pieces that have been edge-bonded. For timber manufactured from multiple-piece laminations (across width) that are not edge-bonded, the  $F_{vy}$  value shall be multiplied by 0.4 for members with 5, 7, or 9 laminations or by 0.5 for all other members. This reduction shall be cumulative with the adjustment in footnote (f).
- (h) The tabulated E values include true E (also known as "shear-free E"), apparent E, and E for beam stability calculation. For calculating beam deflections, the tabulated E<sub>app</sub> values shall be used unless the shear deflection is determined in addition to bending deflection based on the tabulated Etrue. The axial modulus of elasticity, E<sub>axial</sub> and E<sub>axial min</sub>, shall be equal to the tabulated Ey true and Ey min values.
- (i) The values of F<sub>by</sub> were calculated based on members 12 inches in depth. For depths other than 12 inches, the F<sub>by</sub> values are permitted to be increased by multiplying by the size factor (12/d)<sup>1/9</sup>, where d is the beam depth in inches. When d is less than 3 inches, use the size adjustment factor for 3 inches
- (j) The beam depths for 30F-E2M3/SP are limited to 71/4 to 48 inches. The beam depths for 30F-E/DF2 are limited to 71/4 to 26 inches. The 30F-E2M3/SP and 30F-E/DF2 are limited to dry-use only due to the use of LVL tension laminations.
- (k) The F<sub>c,x</sub> value shall be permitted to be increased to the published value of the outermost LVL in the plank orientation.
- (I) The allowable shear stress shall be reduced to 255 psi, 215 psi, and 210 psi, respectively, for 91/4-inch, 71/2-inch, and 71/4-inch-deep beams.

# TABLE 2 – REFERENCE DESIGN VALUES FOR STRUCTURAL GLUED LAMINATED TIMBER<sup>(a,b)</sup> (MEMBERS STRESSED PRIMARILY IN AXIAL TENSION OR COMPRESSION)

(MEMBERS STRESSED FRANKE FERSION OR SOME RESSES)																
Combination Symbol	Species <sup>(c)</sup>	Grade		All Loading	Compression	Axially L	Axially Loaded  Tension		Bending about Y-Y Axis Loaded Parallel to Wide Faces of Laminations				Bending About X-X Axis Loaded Perpendicular to Wide Faces of Laminations		Fasteners	
			Modulus of Elasticity <sup>(d)</sup>			Perpendicular to Grain	Parallel to Grain	Compression Parallel to Grain		Bending <sup>(e)</sup>			Shear Parallel to Grain <sup>(f,g)</sup>	Bending <sup>(h)</sup>	Shear Parallel to Grain <sup>(f)</sup>	Specific Gravity for Fastener Design
						Fcl	2 or More Lami- nations	4 or More Lami- nations	2 or 3 Lami- nations	4 or More Lami- nations	3 Lami- nations	2 Lami- nations	Fvy	2 Lami- nations to 15 in. Deep <sup>(i)</sup>	F <sub>vx</sub>	O
			Ex true, Ey true <b>or</b> Eaxial (10 <sup>6</sup> psi)	Ex app Or Ey app (10 <sup>6</sup> psi)	Ex min, Ey min <b>or</b> Eaxial min (10 <sup>6</sup> psi)	(psi)	F <sub>t</sub> (psi)	F <sub>c</sub> (psi)	F <sub>c</sub> (psi)		F <sub>by</sub> (psi)		(psi)	F <sub>bx</sub> (psi)	(psi)	
1 2 3 5 69 70	DF DF DF AC AC	L3 L2 L2D L1 L3 L2	1.6 1.7 2.0 2.1 1.3 1.4	1.5 1.6 1.9 2.0 1.2 1.3	0.79 0.85 1.00 1.06 0.63 0.69	560 560 650 650 470 470	950 1250 1450 1650 725 975	1550 1950 2300 2400 1150 1450	1250 1600 1900 2100 1100 1450	1450 1800 2100 2400 1100 1400	1250 1600 1850 2100 975 1250	1000 1300 1550 1800 775 1000	230 230 230 230 230 230 230	1250 1700 2000 2200 1000 1350	265 265 265 265 265 265	0.50 0.50 0.50 0.50 0.46 0.46
Wet-use factors			0.833			0.53	8.0	0.73		0.8			0.875	0.8	0.875	See NDS

#### For SI: 1 psi = 6.895 Pa

- (a) The combinations in this table are applicable to members consisting of 2 or more laminations and are intended primarily for members stressed in axial tension or compression. However, design values are tabulated for loading both perpendicular and parallel to the wide faces of the laminations.
- (b) The tabulated allowable design values are for normal duration of loading. For other durations of loading, see applicable building code. The tabulated allowable design values are for dry conditions of use. For wet conditions of use, multiply the tabulated values by the factors shown at the bottom of the table.
- (c) The symbols used for species are AC = Alaska cedar and DF = Douglas fir-larch.
- (d) The tabulated E values include shear-free (true) modulus of elasticity (E<sub>x true</sub>, and E<sub>axial</sub>, apparent modulus of elasticity (E<sub>x app</sub> and Ey app), and 5th percentile modulus of elasticity (E<sub>x min</sub>, Ey min, and E<sub>axial min</sub>). For column stability calculation, E<sub>axial min</sub> shall be used. For calculating the total deflection due to bending, the tabulated Ex app or Ey app values shall be used, or as an alternative, the true (shear-free) bending deflection shall be calculated using the tabulated Ex true or Ey true, which shall be added to the calculated shear deflection to determine the total deflection due to bending.
- (e) The values of F<sub>by</sub> are based on members 12 inches in depth. For depths less than 12 inches, F<sub>by</sub> shall be permitted to be increased by multiplying by the flat use factor, (12/d)<sup>1/9</sup>, where d is the beam depth in inches. When d is less than 3 inches, use the size adjustment factor for 3 inches.
- f) For non-prismatic members, notched members, members subject to impact or cyclic loading, or shear design of bending members at connections, the tabulated Fvx and Fvy values shall be multiplied by 0.72.
- (g) The tabulated F<sub>vy</sub> values are for members of 4 or more lams. The tabulated F<sub>vy</sub> values shall be multiplied by a factor of 0.95 for 3 lams and 0.84 for 2 lams. For members with 5, 7, or 9 lams manufactured from multiple-piece lams with unbonded edge joints, the tabulated F<sub>vy</sub> values shall be multiplied by a factor of 0.4. For all other members manufactured from multiple-piece lams with unbonded edge joints, the tabulated F<sub>vy</sub> values shall be multiplied by a factor of 0.5. This adjustment shall be cumulative with the adjustment specified in Footnote (f).
- (h) The values of  $F_{bx}$  are based on members  $5^{1/8}$  inches in width by 12 inches in depth by 21 feet in length. For members with a larger volume,  $F_{bx}$  shall be multiplied by a volume factor,  $Cv = (5.125/b)^{1/x} (21/L)^{1/x}$ , where b is the beam width (in.), d is the beam depth (in.), L is the beam length between the points of zero moment (ft), and x = 20 for Southern pine and x = 10 for other species.
- (i) The tabulated F<sub>bx</sub> values are for members without special tension lams up to 15 inches in depth. If the member depth is greater than 15 inches without special tension lams, the tabulated F<sub>bx</sub> values must be multiplied by a factor of 0.88. If special tension lams are used, the tabulated F<sub>bx</sub> values are permitted to be increased by a factor of 1.18 regardless of the member depth, provided that the increased F<sub>bx</sub> value does not exceed 2,400 psi. This factor shall be cumulative with the volume factor, C<sub>v</sub>, specified in Footnote (h).



# **ICC-ES Evaluation Report**

# **ESR-5752 City of LA Supplement**

Issued May 2025

This report is subject to renewal May 2026.

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DIVISION: 06 00 00—WOOD, PLASTICS AND COMPOSITES

Section: 06 02 00—Design Information Section: 06 18 13—Glued-Laminated Beams

**REPORT HOLDER:** 

**ROSBORO COMPANY, LLC** 

**EVALUATION SUBJECT:** 

**GLUED-LAMINATED TIMBER** 

### 1.0 REPORT PURPOSE AND SCOPE

### Purpose:

The purpose of this evaluation report supplement is to indicate that Rosboro structural glued-laminated timbers (glulams), described in ICC-ES evaluation report <u>ESR-5752</u>, have also been evaluated for compliance with the codes noted below as adopted by the Los Angeles Department of Building and Safety (LADBS).

## Applicable code editions:

- 2023 City of Los Angeles Building Code (LABC)
- 2023 City of Los Angeles Residential Code (LARC)

## 2.0 CONCLUSIONS

The Rosboro structural glulams, described in Sections 2.0 through 7.0 of the evaluation report <u>ESR-5752</u>, comply with the LABC Chapter 23, and the LARC Chapter R301, and are subject to the conditions of use described in this supplement.

### 3.0 CONDITIONS OF USE

The Rosboro structural glulams described in this evaluation report supplement must comply with all of the following conditions:

- All applicable sections in the evaluation report <u>ESR-5752</u>.
- The design, installation, conditions of use and identification of the Rosboro structural glulams are in accordance with the 2021 *International Building Code*® (IBC) and 2021 *International Residential Code*® (IRC) provisions, as applicable, noted in the evaluation report ESR-5752.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as applicable.
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.

This evaluation report supplement expires concurrently with the evaluation report ESR-5752, issued May 2025.

